Final Design

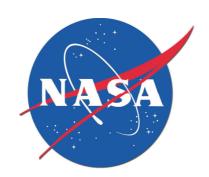
EML 4551C – Senior Design – Fall 2011 Deliverable

Team # 15

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Problem Statement and Project Scope

This senior design project's purpose is to be entered into the Third Annual NASA Lunabotics Competition. This competition goal is to create a robot capable of operating in a lunar environment, including traversing rough terrain, and collecting lunar soil. After the soil is collected, it will be deposited into the LunaBin. This LunaBin will be located 0.35m from the top of the lunar surface. Research on regolith would help determine the feasibility of lunar inhabitance, which could lead to future scientific breakthroughs. The competition will simulate the lunar environment and the accompanying hazards found on the moon, including craters and obstacles for the robot to traverse. Previous competition teams have succeeded with more traditional wheel based design, but have struggled with navigating the obstacles. This year's team will complete with a hexapedal robot based on the RHex family of robots. The main benefit of this design is the ability to easily overcome various obstacles such as rocks and craters via Cshaped legs. Last year's senior design team began building the Hexcavator platform, but was unable to complete the design. The completed portion of the platform is shown below in Figure 1; the platform has a frame, motors, legs, leg attachments and a few other minor components. It has no control system, power system, wireless communication system or excavation system. These systems have been designed and are outlined in detail in this paper.

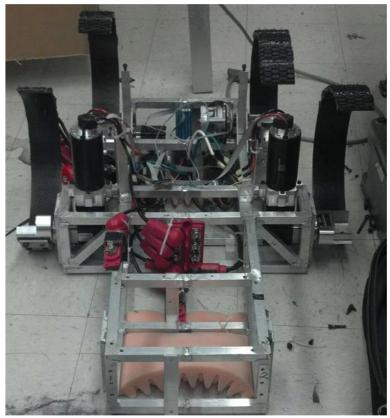


Figure 1: The platform last year's senior design team designed.

Design Requirements

The design requirements of the robot are dictated by NASA's Third Annual Lunabotics Mining Competition Rules and Rubrics ^[3]. Below is a synopsis of these rules, the complete set can be found in the Appendix.

- The competition will take place on May 21-26, 2012. All teams must arrive at the Competition by noon on May 22, 2012.
- The team will be required to complete two, ten-minute competition attempts using the defined competition area provided by NASA.
- The NASA judges need to be able to send an immediate power-off command to the robot at the end of the ten minute competition attempts.
- The robot must excavate at least 10kg of regolith and deposit it into the LunaBin.
 - The LunaBin will be 0.5m tall and have an opening 1.65m long and 0.48m wide.
- The robot must be able to start from any start position dictated by the judges.
- The robot has a weight maximum of 80kg.
- The robot has a starting height maximum of 0.75m.
- The robot has a starting length maximum of 1.5m.
- The robot has a starting width maximum of 0.75m.
- The complete system must be self-powered.
- The team must have one person on the competition team per 23kg of mass of the robot.
- The team must be capable of setting up the robot in the competition area within ten minutes.
- The robot cannot be anchored to the Luna Surface prior to the competition attempt.
- The robot cannot use the walls as support, or use them to push/scoop regolith.
- The robot is limited to autonomous and telerobotic operations only.
- A red emergency stop button of 5cm diameter is required on the exterior of the robot. IT must act as a kill switch and be a commercially bought product.
- The robot is not allowed to use any fundamental physical processes (e.g. suction or water cooling in the open lunar environment), gases, fluids, or consumables that will not work in a lunar environment.
- The robot cannot cause the regolith to undergo any physical or chemical changes, and it may not be treated as a projectile.
- The robot must be able to overcome simulations of obstacles and craters during locomotion.

Design and Analysis

WiFly

To simulate controlling a robot which is located on the moon, NASA uses a control center and provides a wireless signal with a realistic delay. Teams are required to bring their own router and be capable of communicating wirelessly. To complete this task the robot must be capable of receiving wireless signals and subsequently interpreting them. There are several WiFi communication devices available on the market; however few met the specifications necessary for our robotic system. Since the selected microcontroller will have RS232/485 and USB ports, a device with those connectors is required. The STRIDe Lab, an advisor of this project, has several research assistants who have built robots which communicate wirelessly. These researchers recommended the use of a Spark Fun's WiFly module. Due to our limited connector options and the resources which are available for assistance, Spark Fun's WRL-10050 WiFly module was selected.

The WiFly is a standalone wireless networking module; this means that it can both receive and transmit data. A flow chart of the information flow can be seen below in Figure 2. Bi-directional data flow is crucial since commands are going to be sent to the robot and the status will be received from the robot. The main functionality of the WiFly will be to take the user's commands and distribute them to the robot. The user will instruct the robot to either move forward, backward, turn left or turn right. If there is some failure on the robot, the WiFly will transmit back to the user, informing him or her of the error. Since the WiFly is only a standalone serial module, accessing the ports is difficult. However, Spark Fun has a WiFly breakout board, WiFly GSX Breakout, which will make connecting to the chip easier. This breakout board comes with the WiFly attached, so no soldering will be required. The device communicates using a UART port. It can transmit and receive data at speeds up to 1MBps, which will be more than enough for the competition. It uses 33.3 mA at 3V when both transmitting and receiving. The dimensions are 30.48 x 45.72 x 3.5mm. The price of the WiFly with the breakout board is \$84.95 ^[6].



Figure 2: A flow chart demonstrating how the WiFly will send communications from the User in the command center to the Hexcavator and back.

Once the WiFly has been received we will work on basic interfacing with this device. SparkFun's website has several guides and tutorials for setting up the WiFly module. Once a basic configuration is establish, the next goal will be to wirelessly control an LED that is hooked up to one of the output pins of the WiFly. This will demonstrate basic communication with the WiFly. Once a single output can be controlled, the next step would be to have multiple outputs be controlled. This will simulate the various commands that will be sent to the robot: forward, backward, turn left, and turn right. Once the outputs can be varied, the WiFly will be connected to the micro-controller, which will be discussed later in this deliverable.

Power System Power System

The power system components were selected by the previous year's design. The 37V batteries will output approximately 42V when fully charged, these will be run in parallel to double the output current. These batteries will power the voltage regulators, motor drivers, PC/104 microcontroller, Baby O and the motors, demonstrated by Figure 3. The red lines indicate constant voltage supply. The blue lines leading from the motor driver to the motors indicate that the motors will be receiving variable voltage to affect the speeds they turn at. Also, there are actually three motor drivers which control three motors each. This will be discussed in further detail in the controls section of this paper. There are no negative or ground terminals because everything on the robot can use the frame as a common ground.

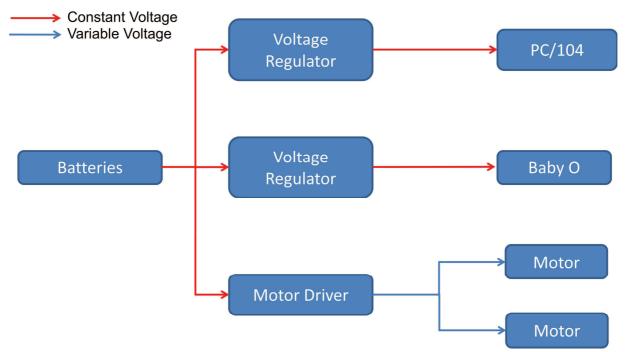


Figure 3: Flow of Positive voltage from batteries to subsystems.

To provide power to the onboard electronics the voltage will be suppressed to 5V using a voltage regulator. One electrical system is more simplistic and makes the power design more streamlined. As an added bonus, the power consumption of our robot can be computed in real time. If the resistance of the circuit is known and a current meter is placed on one side of the batteries, the power consumption can be accurately measured at any one point in time. If these points are added together the total power consumed by the robot can be determined. This measurement is significant because teams are rewarded with points for providing real-time power consumption values and for transmitting the used power data back to base.

The Motor drivers selected are H-Bridge motor drivers capable of providing more than enough current to the motors, which are Maxon RE-65 motors, which are rated for 18V and 296A starting current ^[5]. These also have an attached gear box with a ratio of 50:1. The H-Bridge motor drivers supply the motors with a variable. The ability for the motor drivers to control voltage will be key to controlling the motors speed. Some safety measures have been

implemented including a red safety button that will provide the competition referees with the ability to instantly shut off the robot in the case of an emergency. As per NASA requirements this is an off-the-shelf, unmodified, red, safety switch hardwired which is capable of terminating the robot's power supply with one push. There are also a multiple fuses which will limit the amount of current that is drawn by our motors. If the robot attempts to draw more than 100A, the fuse will blow which will mean all the energy utilized to move a leg will be disconnected.

To test the proposed power system, a Simulink model, shown below in Figure 4 was constructed to test the necessary torque load and current draw the motor will need. Using this model, several graphs were developed demonstrating various scenarios the robot will undergo using quasi-static assumptions.

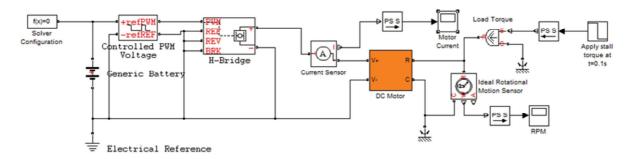


Figure 4: Single leg power diagram for one leg. This incorporates load torque and allows for feedback torque.

Figure 5 shows the current spike that the motor will require when it stalls. It has a maximum current pull of 260 Amps and a load torque of 14 N*m. This plot was chosen because it shows the maximum amount of current that can be used by the motor.

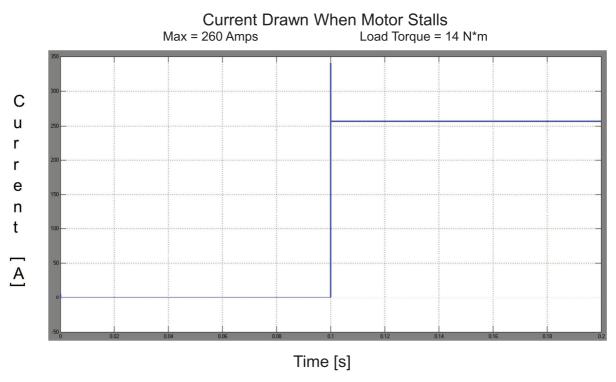


Figure 5: Current draw when the motor stalls.

Hexcavator's nominal position is lay flat on its underside, shown later in Figure 18. It uses all six legs rotating at once to stand up. As the point of contact of the leg to the ground moves closer to the upright position the C-legs will increase in length but the moment will decrease. The current draw on the motor when the robot is standing up is represented below in Figure 6. This figure used a mass estimation of the robot as 76.5 kg, which includes a payload of 9.764 kg of regolith and the excavation system.

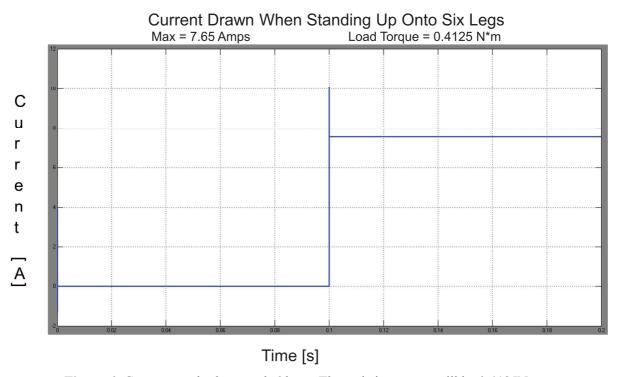


Figure 6: Current required to stand, 6 legs. The resistive torque will be 0.4125Nm.

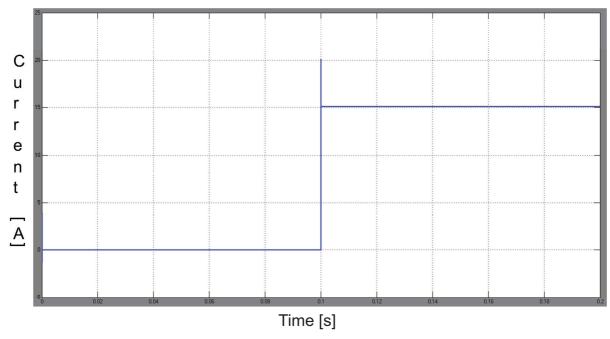


Figure 7: The above graph shows that the current draw at the motor when the Hexcavator is standing on three legs is 15Amps.

Figure 7 represents the amount of current required to stand using only three legs. As the graph demonstrates, the motors draw approximately 15Amps in order to simply stand on three legs. The batteries are capable of providing this amount of amps and the motor is capable of handling this amount of current.

The only part that was unable to be simulated is the discharge rate of the batteries. Provided that the robot isn't heavy enough to stall a motor, from the simulations it can be inferred that the batteries that are more than sufficient to power the robot and are ready to be mounted on the robot

Control

Buehler Clock

One of the challenges encountered on the moon is the terrain, which is full of craters, rocks and other challenging obstacles. The benefit of the RHex platform is its ability to climb over most obstacles instead of avoiding them. All of the obstacles that will be present in the competition will be easily manageable because of the large C-leg design of Hexcavator. However, locomotion for a RHex platform is not as simple as it would be for a traditional wheeled vehicle. The leg rotates about its center axis, creating a circular path. Since this robot is a walking robot, there must be three legs in contact with the ground at all times (this will be discussed in further detail in a later section). As such, the leg must be in contact with the ground for the same amount of time it is in the air. However, the amount of distance the leg must travel in the air is much greater than the distance it must travel when the leg is in contact with the ground. This discrepancy is demonstrated by Figure 8.

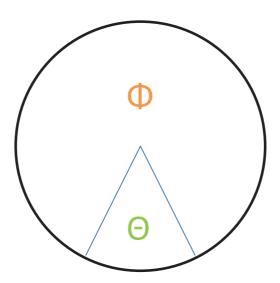


Figure 8: A circle demonstrating the path the leg must cover, and how it is done by a Buehler Clock.

To correct for this discrepancy, the velocity of the leg cannot be the same for the phases indicated by Figure 8. The velocity of leg as it travels through section Θ must be proportionally smaller than the velocity of the leg as it travels through section Φ in order for the time elapse in both states to be equal. As such, a Buheler Clock is used for locomotion. A Buehler Clock is a way of setting speed depending on the position of the motor. Since both angles Θ and Φ will be both known, the factors to adjust the speed, n and m, can be calculated by using the following equation:

 $t(\theta) = n * \theta = m * \Phi = t(\Phi)$ **Equation 1:** Buehler Time Equation In order to implement this, a motor with an encoder is required so that the position can be detected. Once the position is read, the speed of the motor can be adjusted appropriately.

In the current simulations for the robot, a value of 60° and 300° were used for Θ and Φ , respectively. That means that the angular velocity in the Φ sector is five times faster than when in the Θ sector. These degrees may slightly change when implemented on the robot, but should be very close to these values.

Motor Controller

To implement a Buhler clock on Hexcavtor's legs, a control law will be used which will be implemented via a motor controller. Since there are currently no commercially available motor controllers that are capable of implementing a Buheler clock, a custom made one will be used. The design for this motor controller contains three main components: a microcontroller, a motor driver, and a decoder.

The microcontroller will communicate with the PC104 to implement the control law, as demonstrated below in Figure 9. It will also send signals to the decoder to gain information from it about the position and angular velocity of the leg. This information is then fed through the control law which will control the speed of the motor.

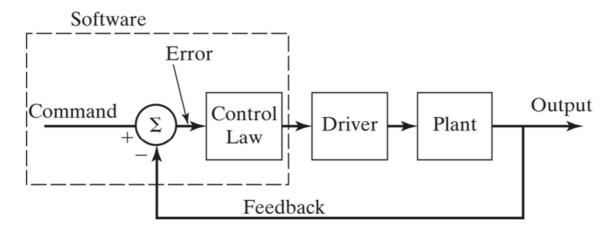


Figure 9: Model of the how the control system will be implemented.

The motor drivers will use an Intersil HIP4081A bridge driver, made by OSMC. It is a dual channel voltage control driver which amplifies the 0V – 5V PWM signal from the microprocessor to a 36V signal. The driver is capable of supplying 150A continuously to two different motors and a maximum short term range of 300A. The current is also reversible so the robot will be able to walk backwards. The lower level control of the legs will be done by the ATmega328P micro-processor mounted in a Pololu Baby Orangutan B-328 (Baby O), shown in Figure 10. Each micro-processor will be utilized to communicate to the motor drivers of two legs, meaning three will be necessary for the operation of the legs of the robot. The micro-processor will output a 5V PWM signal, which will be used as the input to the motor drivers.

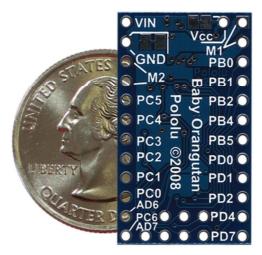


Figure 10: Pololu Baby Orangutan B-328 (Baby O) compared to the size of a quarter.

		BYTE SELECTED			
SEL1	SEL2	MSB	2ND	3RD	LSB
0	1	D4			
1	1		D3		
0	0			D2	
1	0				D1

Figure 11: Byte Selection from the Baby O to the decoder.

Each of the motors is connected to an incremental 512 count per revolution quadrature encoder. Between the leg and the motor there is a 50:1 speed reduction gear box. This gives an overall total of 102400 counts per revolution of the leg. The encoder will be read by an Avago HCTL2023-SC decoder chip. This chip reads up to a 32bit count at 32MHZ. This will be more than adequate for the needs of the robot. The Baby O will communicate with the decoder chip using 12 different analog control lines. Because there are 4 bytes that need to be read, 2 lines are used to select what byte will be read. As shown in Figure 12, one line is used to control what motor's position will be read. The decoder is a dual channel decoder so it is capable of reading both motors that the Baby O will be controlling. A final line is used to tell the decoder to reset. 8 lines are used to as an output from the decoder. They are the lines that are held high or low to determine each of the 4 bites. These lines are then interpreted by the Baby O to find the current position of the motor.

Using the position of the motor a control law is enacted. The control law will control the speed of the motor based on the position of the leg. It will also enact a Buhler clock on each of the legs. A Buhler clock is used when the speed of the leg throughout the stride is not constant.

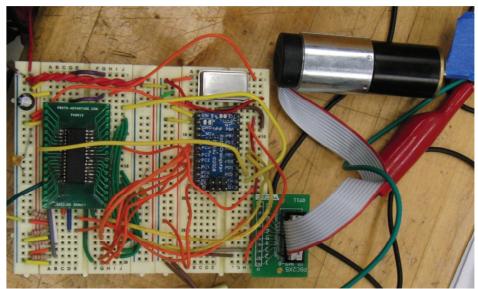


Figure 12: Prototype motor controller with a small DC motor. The Baby O was capable of implementing a control law implement a Buheler clock onto the DC motor.

As shown in Figure 12 a prototype motor-controller was constructed that was used to drive a smaller motor. A control law was also successfully implemented to make the motor turn in a Buhler clock motion. This was a successful proof of concept test. The next step in this design is to produce a printed circuit board or PCB that is capable of connecting all the devices used in the controller. The bread board and jumper wire setup was successful for testing however a PCP setup will be much more reliable and sustainable for the final robot.

During testing the Baby O was capable of closing the loop at a rate of 3kHz. This is very good and will be more than adequate for use on the robot in final competition. The only feature that the motor-controller does not have is the ability to detect how much current is being consumed by the motors. This problem will be solved by adding an inline current meter to the final controller. A Honeywell CSNF151 will be added between the battery and the motor drivers, this will output an analog voltage signal proportional to the current being consumed by the whole system. This signal will be used to determine in real time if there is a failure in the system and also for scoring purposes for the competition.

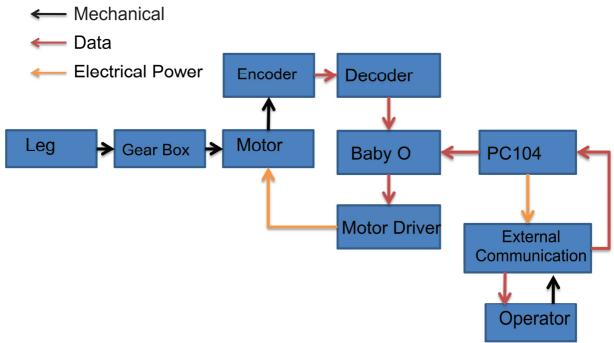


Figure 13: Flow chart representing how information will be elicited from the robot. It will be iterated in each of the six legs.

Micro Controller

The two final ideas for the robot's main controller were a netbook or a PC/104 microcontroller. While the netbook is easy to interface, it does not have any serial connections which are an essential for communication with the other parts of the robot. Though USB to RS232 connectors exist, netbooks typically come with two to three USB ports. Each set of legs is going to require a RS232 port to communicate with the netbook. While there would be enough ports for each of the legs, this leaves no way to communicate with the excavation or any other additional system that may be added. If a USB hub was added to the netbook, this would increase the number of USB ports, but communicating becomes less trivial. This extra work required to go through the USB Hub offsets the initial perk. Additionally, the reliability of USB to RS232 connectors is questionable at best. Lamment Bies, a Software Managing Director, said this about the potential downfalls of the conveters, "This non-standard behaviour of RS232 inputs makes it even more difficult to select the right RS232 to USB converter. If you connect and test an RS232 to USB converter over a serial line with another device, it might work with some devices, but not with others[SM1]." Meanwhile, the PC/104 allows low level communication through serial ports, but will be labor intensive to program. However, the vendor from which the PC/104 is being purchased, Advantech, supplies their own version of Windows XP for the micro-controller. This will cut down the amount of time required to learn how to interface with the PC/104 and will provide us with a resource when problems arise. Not only does the vendor supply an operating system for the board, but they also supply drivers for the various stacks that will be used with the robot. This decreases the interfacing issue with the PC/104. Ultimately, the PC/104 was found to be the optimal component for the project, due to its ability to communicate through serial ports.

The PC/104 will act as the liaison between the user and the robot. The user will command the robot to either to move, stop, excavate, dump, etc. through the WiFly module. This command will be interpreted by the PC/104. Once the PC/104 has the user's command, it will command the motor communication system with what speed to obtain. In the unfortunate situation in which there is a malfunction with one of the legs, the motor-communications system would inform the PC/104, which will then tell the user of the error. This communications system can be seen in Figure 14:

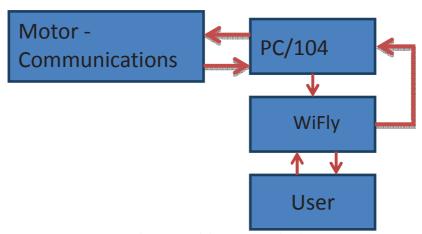


Figure 14: Basic Setup of the Communications System.

The PC/104 selected has three separate modules: the main micro-controller, the additional serial port module and a digital I/O module. The micro-controller that was selected was the Advantech PCM-3355. It features an AMD Geode LX 800 processor, which has a frequency of 500MHz. The operating system for our robot will be Windows Embedded CE 6.0. It requires 2GB of storage space to install. Since the memory comes in either 1GB, 2GB, 4GB or 8 GB, a 4GB hard disk was selected. Since the only thing that will be on the PC/104 is the operating system, drivers for the other modules and the code to run the PC/104, 4 GB will be more than sufficient. It comes with 512MB of RAM but is capable of being expanded to 1GB. Both the hard drive and RAM will be comprised of flash memory. A hard disk drive would be undesirable for this application, due to the potential of regolith getting inside of the moving parts. The module typically draws 1.45A at +5V. The main micro-controller comes with one RS485 connector, which is sufficient for communication with the WiFly. It also has two RS232 connectors, which means an additional serial module is required for complete communication with the robot. The Advantech PCM-3644 has four RS232 slots and four RS485 slots. The additional serial ports will allow communication with the other motor control systems. The digital I/O module that has been selected is the Advantech PCM 3724, which has a total of 48 channels. The ports operate using TTL of 5V. These digital I/O ports will be used to control the excavation system and may be useful in the future development of the robot. The typical power consumption of the PCM-3644 is 400mA at +5V. The micro-controller, PCM-3355, has physical dimensions of 96 x 90 x 19.3 mm and a weight of 0.097kg. The serial extension, PCM-3644, has physical dimensions of 96 x 90 x 18.9 mm and a weight of 0.084kg. Finally, the PCM- 3724 has dimensions of 96 x 90 x 19.1 mm and weighs 0.073 kg. Since the three modules are meant to stack upon one another, the final dimensions, when assembled, are 96 x 90 x 57.3mm and a weight of 0.254kg. The cost of the micro-controller, PCM-3355, with the operating system is \$365. The cost of the serial module, PCM-3644, is \$144. The cost of the digital I/O module, PCM-3724, is \$79. The total cost of these modules is \$691.

An incremental engineering approach will be taken when testing the PC/104. The first test will be to turn on a LED that is connected to one of the PC/104's output pins depending on the reading from the serial port. This will simulate receiving an input from the WiFly and exporting a signal to digital I/O ports. After the PC/104 is communicating, modules can be added to the system to be tested. The first module that will be added is the WiFly. The first test will be redone, but this time there will be wireless communication, as opposed to hardwired. Once wireless communication has been established to the PC/104, the next step would be to control the direction of the motor with a wireless signal. Once wireless communication and motor control have been proven, this design can be implemented on the actual robot.

Center of Mass

The Hexcavtor walks using an alternating tripod gait, which is based on how cockroaches walk. It is demonstrated in Figure 15; the left image uses red and blue dots to indicate a set of legs that move together, the right image is a ProEngineer depiction of a tri-pod gait. Essentially, there are two sets of three legs. The legs in the set all move together. When the first set (red dots) are touching the ground, the second set is in the air. When the first set of legs lift off the ground, the second set will come down so there will always be at least three legs on the ground. This means the Hexcavator will never enter an aerial phase, since it would always be touching the ground during locomotion. The control of the legs will be discussed in a later section.

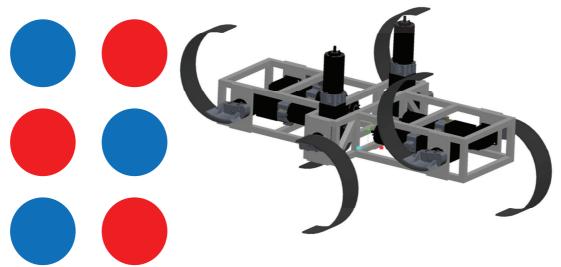


Figure 15: (Left): The dots depict what which legs move together during an alternating tri-pod gait. When the first set of legs are touching the ground (red dots) the second set (blue dots) are in the air. When the first set lifts off the ground the second set will touch the ground. (Right): A ProEngineer rendering of what the robot will look like while walking.

Since the robot will never be in an aerial phase the center of mass will be triangulated using the legs. When one set of legs is touching the ground, the center of mass must be contained in the purple triangle shown below in Figure 16. When the other set of legs is touching the ground the center of mass must be contained within the red triangle. Therefore the center of mass must be contained within the blue hexagon to satisfy the gait. A simulation of the location of the center of mass was completed using ProEngineer, show in Figure 17. This simulation assumed that the drum was filled with the maximum amount of regolith the drum could hold, 9.761 kg, since the known density of regolith is $1.5g/cm^3$. The excavation system is represented in the position it will be at while the robot is walking.

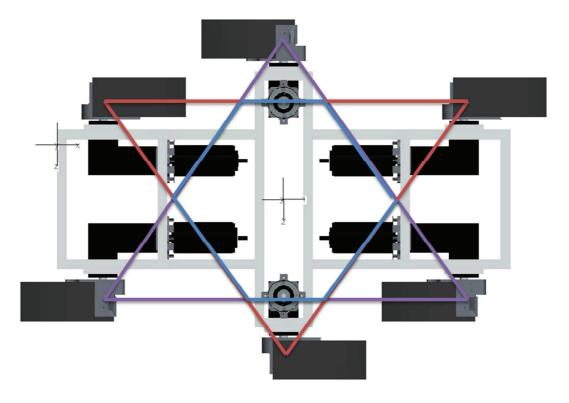


Figure 16: When one set of legs is touching the ground, the center of mass must be contained in the purple triangle. When the other set of legs is touching the ground the center of mass must be contained within the red triangle. As such the center of mass must be contained within the blue hexagon.

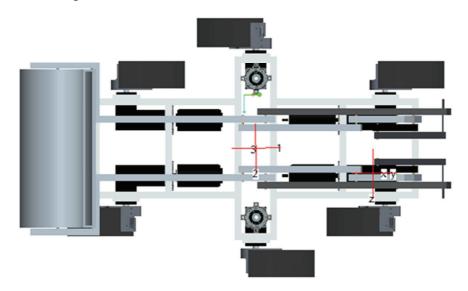


Figure 17: Center of mass simulation when the excavation drum contains the maximum amount of regolith. Regolith has a density of $1.5g/cm^3$ and the drum can hold a maximum of 9.761kg regolith.

The competition evaluates the dimensions and mass of the robot prior to the competition. To begin the Hexcavator will be laying down on its underside and the excavation system will be in the position shown in Figure X. This gives the robot a starting height of 38.97cm, length of 123.01cm, width of 75cm, and mass of 67kg as simulated in ProEngineer. These dimensions are all within the competition limitations.

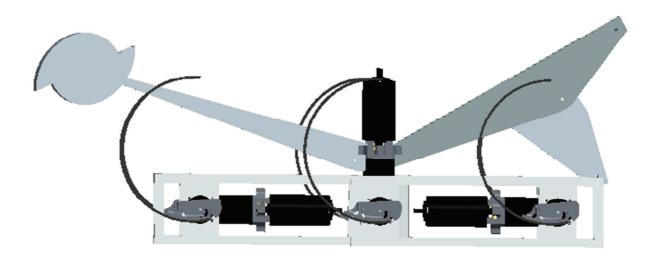


Figure 18: Initial position of the excavation system; this is the position the robot will be measured in to ensure it meets the competition standards, however the robot will be sitting at start to make sure it meets these requirements.

Excavation

The purpose of the competition is to excavate at least 10kg of regolith from the excavation area and deposit it in the LunaBin at the opposite end of the competition area, depicted in Figure 19. The LunaBin and its dimensions are shown in more detail in Figure 20.

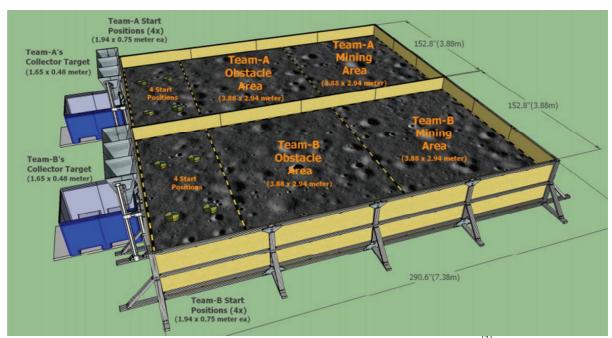


Figure 19: The competition area the robot will be competing $in^{[3]}$.

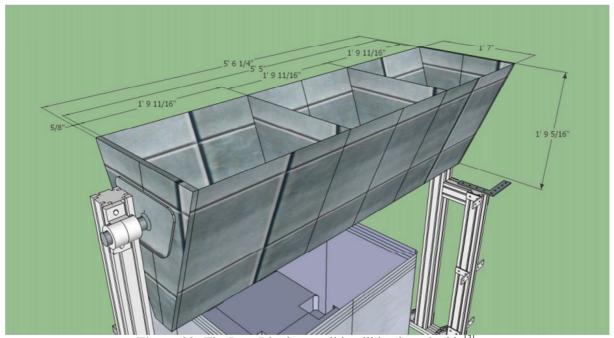


Figure 20: The LunaBin the regolith will be deposited in [3].

Excavator

Regolith is notoriously a very dense, sticky material which becomes compacted and gets into all crevices. To mitigate this concern the excavator will be a rotating drum with slits on each end which will cut into the excavating surface, shown in Figure 21. The drum can hold a maximum of 9.764 kg regolith and will be made of Aluminum 6061 (a detailed drawing of it can be found in the Appendix). Since the minimum amount of regolith that needs to be excavated and deposited in the LunaBin is 10kg, the robot will be easily able to complete its required task. Aluminum 6061 was chosen because of its low density compared to other metals, while maintaining and the necessary hardness. The diameter of the rotating drum is 9inch and it is 18inch wide. When the robot is walking the linkage will hold the excavation system in such a position that the center of mass of mass will be within the necessary bounds, as indicated in Figure 22. When the robot is in excavating the robot will kneel down on its front legs to enhance stability as demonstrated in Figure 23. The rotating drum will be lowered to the surface and it will rotate so it will break the compacted surface and scoop the regolith into the drum. When the drum is full the robot will raise the excavation system back over the center of mass demonstrated again in Figure 24. Then the robot will stand back up and navigate to the LunaBin. When it gets to the Lunabin, the robot will bring the excavation drum over the LunaBin, depicted in Figure 25. Then the drum will then counter rotate and release the regolith into the LunaBin. Then the linkage will guide the excavation system back over the center of mass and the Hexcavator will stand back up and repeat the process.

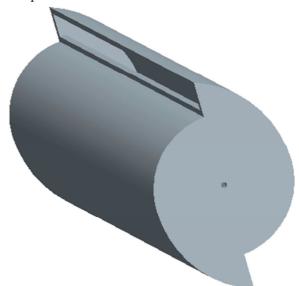


Figure 21: The rotating drum which will be used to excavate lunar regolith. It can hold a maximum of 9.764 regolith.

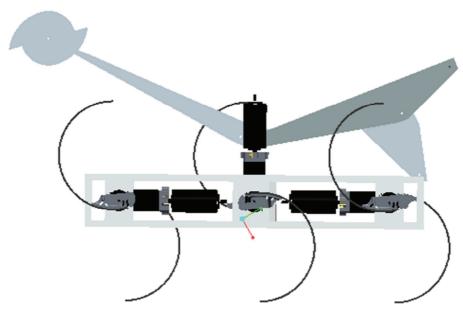


Figure 22: Hexcavator in its walking position. This is the same position the robot will be measured in at the beginning of the competition.

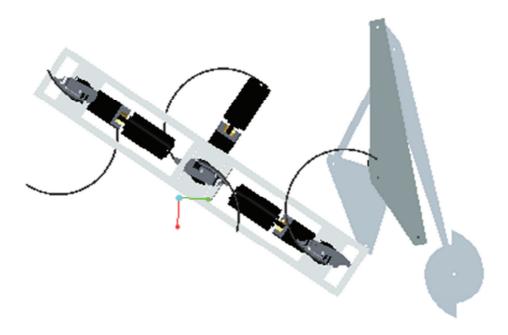


Figure 23: The robot in the excavating position. The robot will be laying on its underside to enhance stability while excavating regolith.



Figure 24: The excavation system located close to the center of mass for walking across the competition area.

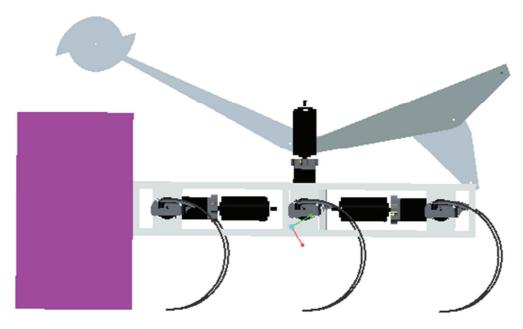


Figure 25: Hexcavator's position when it is depositing regolith in the LunaBin. The purple rectangle represents the LunaBin the regolith will be deposited in.

Linkage

The linkage used to attach the excavation system to Hexcavator is a six-bar linkage made from Aluminum 6061, shown in more detail below in Figure 26. The six bar was chosen because of it versatility of movement. Though the Hexcavator platform is capable of turning around, this system will allow for the robot to simply traverse forwards and backwards across the arena saving time. Since the robot can walk backwards this is an elegant solution to save time.



Figure 26: Close up image of the six-bark linkage design which will be utilized to move the excavation drum.

The required torque to move the linkage when the drum is both empty and full of regolith are shown below in Figure 27, which is a ProEngineer torque analysis of the system. These graphs were converted to show that when there is no regolith in the drum, the linkage will need 38N*m of torque to rotate and when the drum is holding the maximum capacity of regolith, the linkage will need 61N*m of torque to rotate.

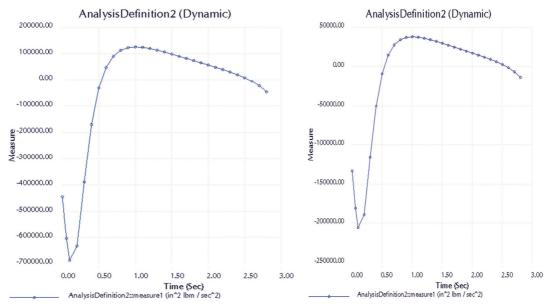


Figure 27: (Left) Pro Engineer analysis of the amount of torque necessary to rotate the six bar linkage when the excavation drum is empty (38Nm). (Right) Pro Engineer analysis of the amount of torque necessary to rotate the six bar linkage when the excavation drum contains the maximum amount of regolith (61Nm).

Hardware

The bearings chosen for the linkage are PTFE/Oil-Lubricated SAE Bronze Flanged Sleeve Bearings manufactured by McMaster-Carr, which cost \$0.64 each; our six bar design will require 24 of them ^[4]. Flanged bearings were selected to act as spacers between the links and better hold them in place. They have been added to the ProE assemble shown in Figure 24 and are shown below in Figure 28. The pins used will be hardened steel (1566 steel), ¹/₄" diameter which can be purchased from McMaster-Carr ^[4]. To hold the shafts inside the linkage, CirClips will be used. These have a ring thickness of 0.025" and are made of Stainless Steel. Detailed specifications of all these parts are listed in the Appendix.

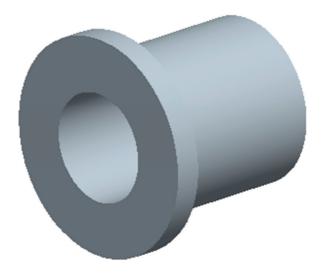


Figure 28: PTFE/Oil-Lubricated SAE Bronze Flanged Sleeve Bearings distributed by McMaster-Carr ^[4]. 24 of these will be used in the six-bar linkage design of Hexcavator.

Drive System

The selected motor to drive the excavation drum is a Robotech NPC T74. It is capable of being run at 36V and has a 20:1 gear ratio. It exceeds the torque requirements of 61N*m. The motor to drive the six-bar was purchased last year.

Cost Analysis

In Figure 29, the breakdown of final cost estimates for individual components are given. Our total budget amounts to \$6000. We received \$2000 from FAMU/FSU College of Engineering and \$4000 from National Space Grant. Our final cost estimate is \$5451.77 which is within our budget. The rest of the budget will be reserved for unanticipated costs that may arise during construction.

Components	Cost	Quantity	Total Cost
Bushings	\$0.64	24	\$15.36
PC104	\$ 691.00	1	\$691.00
Aluminum (Excavation)	\$600.00	1	\$600.00
ABS Plastic (Excavation)	\$30.00	1	\$30.00
Steel Shafts	\$40.00	1	\$40.00
CirClips (Pack of 10)	\$8.09	3	\$24.27
Motor for Excavation	\$359.34	1	\$359.34
WiFly	\$84.95	1	\$84.95
Baby O	\$19.00	5	\$95.00
Motor Drivers	\$220.00	4	\$880.00
Voltage Regulators	\$6.00	5	\$30.00
Decoders	\$8.00	5	\$40.00
Clocks	\$3.00	7	\$21.00
Copper Sheet	\$60.00	1	\$60.00
Travel Expenses (Estimated)	\$2,480.85	1	\$ 2,480.85
Total			\$ 5,451.77

Figure 29: Breakdown of the final cost estimates for the Hexcavator.

Conclusion

Risks Assessment

The two most challenging aspects of this project are the integration of numerous systems and applying an adequate controls scheme. Any system that requires the integration of so many smaller subsystems will be inherently challenging. While the power capabilities of the robot are adequate to provide power to all the subsystems, distributing it correctly will be a challenge initially. Devising a way to communicate from a PC to a WiFly to a Microcontroller and back will also be extremely challenging, especially since such a system is unprecedented. Additionally, the environment consists of regolith, which is very fine. One of the requirements of NASA is to create a regolith resistant design. The reasoning behind this is to protect the mechanical and electrical systems of the robot. Communication between all the systems will pose a difficulty initially. Devising an adequate controls scheme and tuning it will take a significant amount of time, however we are confident that our team is capable of tackling all these challenges. There are numerous resources at our disposal via advising professors and references. There will also be substantial time for testing.

Final Statement

The power simulations show that there will be enough power for the robot for the duration of the competition. Also, since the wireless communication system has been used by our advisors previously we are confident it can be implemented. Our microcontroller should be more than adequate for what we are trying to do with it. Since our controls scheme has already been developed, it will simply need to be tried and tested to optimize it on our final design. As stated previously, the most challenging portion of this project will the integration of all the subsystems.

The six-bar linkage will provide a lot of mobility and as the simulations indicate, it maintains the center of mass well within the bounded areas. Also, our excavation drum should be capable to scraping the regolith surface and carrying a significant payload.

Our safety switches and fuses are in place for safety of Hexcavtor as well as all participants in the competition. All requirements dictated by NASA's rules have been met by our design and our analysis makes us confident in our design. We are looking forward to constructing the Hexcavator and being testing.

Time Line

The team has come up with their own internal goals, which can be seen in the gray rows of the Gantt Chart. They are further explained below:

Research

Completion: Week 5

The team has performed an in-depth analysis of the former year's robot to determine which components can be utilized again for this year (discussed above in the budgeting section). Locomotion schemes, controls and different methods of excavation were reserached. The team agreed on a micro controller and motor controllers, and met with a technical expert, Dr. Camillo Ordonez, to verify that our selected components were suitable.

Prototype 1a: Walking Platform

Intended Completion Date: Week 17

By the end of week 17, the group would like to have a functional walking hexapedial platform. Achieving this will entail acquisition of needed electrical components, installation, programming and testing of the drive system.

Even though the long term goal is for the robot to be controlled via WiFi, an umbilical tether will be used initially for simplicity. Once the robot is mobile, it will be tested indoors. The next step is to test Hexcavator in an outdoor sand pit. This will test Hexcavator's capabilities on non-consistent surface. After testing Hexcavator's ability to go forwards and backwards, the robot will need to be programmed to make turns within the confinements of the competition arena.

Initial Prototype of Excavation

Intended Completion Date: Week 12.

The production of the excavation system will be a multistep process involving design, integration, and improvement. The team developed a six-bar linkage which can be mounted on the existing frame. An excavating drum was also designed as a method of actually excavating the regolith. This design will be prototyped by week 12 from ABS plastic. The experiments will be conducted using sand as a simulant for the regolith. The testing is expected to be complete by the end of week 12.

Prototype 1b: Excavation Design

Intended Completion Date: Week 17

After prototype testing is complete for the excavation design and the excavation design will undergo final changes and will be then machined from Al6061. It will then be mounted to the existing Hexcavator frame (using the mounts constructed by last year's team). The next step will be to implement the motors and a controls scheme onto the excavation system. Then tests will

be conducted in soil to verify that it the design works. The key here is the strength of the excavation system and its ability to dig into the compacted ground. By the conclusion of week 17, the excavation system will be extracting both soft and compacted soil from the ground and will be depositing it into a test bin. Then the

Prototype 2: Wireless Walking Robot with Excavation

Intended Completion Date: Week 22

The Hexcavator will have considerably more mass above the top of the robot when the excavation system is attached. Hexcavator will need to undergo testing and control refinement to maintain its locomotion capabilities. The system will also need to be tested to see if it is still capable of picking up soil. Additional testing will be performed to see how Hexcavator's locomotion is impacted when the excavation system is carrying the regolith. Depositing the regolith simulant will also need to be tested so that the maximum amount will be deposited. Navigating over obstacles will also need to be tested with the additional weight of the excavation system, with and without regolith. During these testing phases a wireless communications system will be implemented so that the robot will not need its umbilical tether.

Prototype 3: Walking Robot in Rough Terrain

Intended Completion Date: Week 29

The final steps that will be tested and practiced on the Hexcavator system will to making sure that the complete system is working correctly and efficiently. This will include navigating all obstacles, such as rocks, craters, and rough terrain. Also, the entire system will need to be capable of collecting soil and traversing a practice course to deposit into a practice bin. The excavation system at this point should be collecting the simulated regolith without hindering locomotion. It will then traverse the practice course to successfully deposit said substitute material into a practice bin that will simulate the LunaBin that will be used during competition. At the end of this deliverable, the team will participate in NASA's competition at Kennedy Space Center on May 23.

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Design control system for excavation	Develop and test a dumping mechanism.	
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Prototype 2: Wireless Walking Robot with Excavation	
Attach Excavation to walking platform.	
Test moving with attached excavation.	
Refine extraction control and mechanism.	
Test depositing soil into bin.	
Make Robot wireless.	
Prototype 3: Walking Robot in Rough Terrain	
Test combined system's ability to navigate obstacles.	
Refine locomotion control for excavation over uneven ground.	
Test picking up soil on uneven ground.	
Prepare for final demonstration.	

Figure 30: Ghant chart for developing the Hexcavator Platform.

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Appendix

Complete NASA Rules	Ai
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NASA's Third Annual Lunabotics Mining Competition

Rules & Rubrics, Revision 2

Kennedy Space Center Visitor Complex Kennedy Space Center, Florida



Introduction

NASA's Lunabotics Mining Competition is designed to promote the development of interest in space activities and STEM (Science, Technology, Engineering, and Mathematics) fields. The competition uses excavation, a necessary first step towards extracting resources from the regolith and building bases on the moon. The unique physical properties of lunar regolith and the reduced 1/6th gravity, vacuum environment make excavation a difficult technical challenge. Advances in lunar regolith mining have the potential to significantly contribute to our nation's space vision and NASA space exploration operations.

The competition will be conducted by NASA at the Kennedy Space Center Visitor Complex. The teams that can use telerobotic or autonomous operation to excavate lunar regolith simulant, called Black Point-1 or BP-1, and score the most points wins the Joe Kosmo Award for Excellence. The team will receive the Joe Kosmo Award for Excellence trophy, KSC launch invitations, team certificates for each member, a \$5,000 team scholarship, and up to \$1,000 travel expenses for each team member and one faculty advisor to participate at one of NASA's remote research and technology tests. Awards for other categories include monetary team scholarships, a school trophy or plaque, team and individual certificates, and KSC launch invitations.

Undergraduate and graduate student teams enrolled in a U.S. or international college or university are eligible to enter NASA's Lunabotics Mining Competition. Design teams must include: at least one faculty with a college or university and at least two undergraduate or graduate students. NASA has not set an upper limit on team members. A team should have a sufficient number of members to successfully operate their Lunabot. Teams will compete in up to five major competition categories including: on-site mining, systems engineering paper, outreach project, slide presentation (optional), and team spirit (optional). Additionally, teams can earn bonus points for mined and deposited BP-1 in the competition attempts, having multidisciplinary teams, and collaborating between a majority institution and a U.S. minority serving institution. All documents must be submitted in English.

The Lunabotics Mining Competition is a student competition that will be conducted in a positive, professional way. This is a reminder to be courteous in all your correspondence and all interactions on-site at the competition. Unprofessional behavior or unsportsmanlike conduct will not be tolerated and will be grounds for disqualification. The frequently asked questions (FAQ) document is updated regularly and is considered part of this document. It is the responsibility of the teams to read, understand, and abide by all of NASA's Third Annual Lunabotics Mining Competition Rules and Rubrics, stay updated with new FAQs, communicate with NASA's representatives, and complete all surveys. These rules and rubrics are subject to future updates by NASA at its sole discretion.

For more information, visit NASA's Lunabotics Mining Competition on the Web at www.nasa.gov/Lunabotics; on Facebook at www.facebook.com/Lunabotics; on YouTube at http://www.youtube.com/user/Lunabotics; and follow Lunabotics on Twitter at http://twitter.com/#!/Lunabotics.

Lunabotics On-Site Mining Category

This year the scoring for the Mining Category will not be based primarily on the amount of material excavated in the allowed time but instead will require teams to consider a number of design and operation factors such as dust tolerance and projection, communications, vehicle mass, energy/power required, and level of autonomy. Each team must compete on-site at the Kennedy Space Center Visitor Complex, Florida in the United States of America on May 21-26, 2012. A minimum amount of 10 kg of BP-1 must be mined and deposited during each of two competition attempts according to the rules to qualify to win in this category. In the case of a tie, the teams will compete in a tie-breaking competition attempt. The judges' decisions are final in all disputes. The teams with the first, second, and third most LunaPoints averaged from both attempts will receive team plaques, individual team certificates, KSC launch invitations, \$3,000, \$2,000, and \$1,000 scholarships and 30, 25, and 20 points toward the Joe Kosmo Award for Excellence, respectively. Teams not winning first, second, or third place in the mining category can earn one bonus point for each kilogram of BP-1 mined and deposited up to a maximum average of ten points toward the Joe Kosmo Award for Excellence. The most innovative and lunar like design will receive the Judges' Innovation Award at the discretion of the mining judges.

1) Teams must arrive at the Lunabotics Mining Competition Check-In Tent in Parking Lot 4 of the Kennedy Space Center Visitor Complex no later than 12:00 p.m. (noon) on Tuesday, May 22, 2012.

Game Play Rules

- 2) Teams will be required to perform two official competition attempts using BP-1 in the LunArena provided by NASA. NASA will fill the LunArena with compacted BP-1 that matches as closely as possible to lunar regolith. NASA will randomly place three obstacles and create two craters on each side of the LunArena. Each competition attempt will occur with two teams competing at the same time, one on each side of the LunArena. After each competition attempt, the obstacles will be removed, the BP-1 will be returned to a compacted state, if necessary, and the obstacles and craters will be returned to the LunArena. The order of teams for the competition attempts will be chosen at NASA's discretion. See Diagrams 1 and 2.
- 3) In each of the two official competition attempts, the teams will score cumulative LunaPoints. See Table 1 for the Mining Category Scoring Example. The teams' ranking LunaPoints will be the average of their two competition attempts.
 - A) Each team will be awarded 1000 LunaPoints after passing the safety inspection and communications check.
 - B) During each competition attempt, the team will earn 2 LunaPoints for each kilogram in excess of 10 kg of BP-1 deposited in the LunaBin. (For example, 110 kg of BP-1 mined will earn 200 points.)
 - C) During each competition attempt, the team will lose 1 LunaPoint for each 50 kilobits/second (kb/sec) of average data used throughout each competition attempt. A minimum of 10 kg of BP-1 must be mined and deposited in the LunaBin during each competition attempt or the team will lose 100 LunaPoints, which is the maximum number of LunaPoints for this rule. (For example, 5000 kb/sec will lose 100 points.)
 - D) During each competition attempt, the team will lose 10 LunaPoints for each kilogram of total Lunabot mass. (For example, a Lunabot that weighs 80 kg will lose 800 LunaPoints.)
 - E) During each competition attempt, the team will earn 100 LunaPoints if the amount of energy consumed by the Lunabot during the competition attempt is reported to the judges after each attempt. The amount of energy consumed will not be used for scoring; a team must only provide a legitimate method of measuring the energy consumed and be able to explain the method to the judges.
 - F) During each competition attempt, the judges will award the team 0 to 200 LunaPoints for regolith dust tolerant design features on the Lunabot and regolith dust free operation. If the Lunabot has exposed mechanisms where dust could accumulate during a lunar mission and degrade the performance or lifetime of the mechanisms, then fewer points will be awarded in this category. If the Lunabot raises a substantial amount of airborne dust or projects it due to its operations, then fewer points will be awarded. Ideally, the Lunabot will operate in a clean manner without dust projection, and all mechanisms and moving parts will be protected from dust intrusion. The Lunabot will not be penalized for airborne dust

- while dumping into the LunaBin. All decisions by the judges regarding dust tolerance and dust projection are final.
- G) During each competition attempt, the team will earn 250 LunaPoints if the Lunabot is able to drive autonomously (no teleoperation), through the obstacle area only. The Lunabot may be teleoperated in the mining area and LunaBin/starting area. A minimum of 10 kg of BP-1 must be mined and deposited in the LunaBin during each competition attempt to receive these LunaPoints. The points for autonomy through the obstacle area and full autonomy are mutually exclusive.
- H) During each competition attempt, the team will earn 500 LunaPoints if full autonomy is achieved and a minimum of 10 kg of BP-1 is mined and deposited in the LunaBin. No teleoperation is allowed to achieve full autonomy status. The points for autonomy through the obstacle area and full autonomy are mutually exclusive.

Mining Category Elements	Specific Points	Actual	Units	LunaPoints
Pass Inspections				1000
Regolith over 10 kg	+2/kg	110	kg	+200
Average Bandwidth	-1/50kb/sec	5000	kb/sec	-100
Lunabot Mass	-10/kg	80	kg	-800
Report Energy Consumed	+100	1	1= Achieved 0= Not Achieved	+100
Dust Tolerant Design & Dust Free Operation	0 to +200	150	Judges' Decision	+150
Autonomy through Obstacles	+250	0	1= Achieved 0= Not Achieved	0
Full Autonomy	+500	500	1= Achieved 0= Not Achieved	+500
Total				1050

Table 1: Mining Category Scoring Example

- 4) All excavated mass deposited in the LunaBin during each official competition attempt will be weighed after the completion of each competition attempt.
- 5) The Lunabot will be placed in the randomly selected starting positions. See Diagrams 1 and 2.
- 6) A team's Lunabot will only excavate BP-1 located in that team's respective mining area at the opposite end of the LunArena from the team's starting area. The team's starting direction will be randomly selected immediately before the competition attempt.
- 7) The Lunabot is required to move across the obstacle area to the mining area and then move back to the LunaBin to deposit the BP-1 into the LunaBin. See Diagrams 1 and 2.
- 8) Each team is responsible for placement and removal of their Lunabot onto the BP-1 surface. There must be one person per 23 kg of mass of the Lunabot, requiring four people to carry the maximum allowed mass. Assistance will be provided if needed.
- 9) Each team is allotted a maximum of 10 minutes to place the Lunabot in its designated starting position within the LunArena and 5 minutes to remove the Lunabot from the LunArena after the 10-minute competition attempt has concluded.
- 10) The Lunabot operates during the 10-minute time limit of each competition attempt. The competition attempts for both teams in the LunArena will begin and end at the same time.
- 11) The Lunabot will end operation immediately when the power-off command is sent, as instructed by the competition judges.

- 12) The Lunabot cannot be anchored to the BP-1 surface prior to the beginning of each competition attempt.
- 13) The Lunabot will be inspected during the practice days and right before each competition attempt. Teams will be permitted to repair or otherwise modify their Lunabots anytime the LunaPits are open.

Field Rules

- 14) At the start of each competition attempt, the Lunabot may not occupy any location outside the defined starting position.
- 15) The LunaBin top edge will be placed so that it is adjacent to the side walls of the LunArena without a gap and the height will be approximately 0.5 meter from the top of the BP-1 surface directly below it. The LunaBin top opening will be 1.65 meters long and .48 meters wide. See Diagrams 1 3. A target may be attached to the LunaBin for navigation purposes only. This navigational aid must be attached during the setup time and removed afterwards during the removal time period. The mass of the navigational aid is included in the maximum Lunabot mass limit of 80.0 kg and must be self-powered.
- 16) There will be three obstacles placed on top of the compressed BP-1 surface within the obstacle area before each competition attempt is made. The placement of the obstacles will be randomly selected before the start of the competition. Each obstacle will have a diameter of approximately 20 to 30 cm and an approximate mass of 7 to 10 kg. There will be two craters of varying depth and width, being no wider or deeper than 30 cm. No obstacles will be intentionally buried in the BP-1 by NASA, however, BP-1 includes naturally occurring rocks.
- 17) The Lunabot must operate within the LunArena: it is not permitted to pass beyond the confines of the outside wall of the LunArena and the LunaBin during each competition attempt. The BP-1 must be mined in the mining area and deposited in the LunaBin. A team that excavates any BP-1 from the starting or obstacle areas will be disqualified. The BP-1 must be carried from the mining area to the LunaBin by any means and be deposited in the LunaBin in its raw state. A secondary container like a bag or box may not be deposited inside the LunaBin. Depositing a container in the LunaBin will result in disqualification of the team. The Lunabot can separate intentionally, if desired, but all parts of the Lunabot must be under the team's control at all times. Any ramming of the wall may result in a safety disqualification at the discretion of the judges. Touching or having a switch sensor springwire that may brush on a wall as a collision avoidance sensor is allowed.
- 18) The Lunabot must not use the wall as support or push/scoop BP-1 up against the wall to accumulate BP-1. If the Lunabot exposes the LunArena bottom due to excavation, touching the bottom is permitted, but contact with the LunArena bottom or walls cannot be used at any time as a required support to the Lunabot. Teams should be prepared for airborne dust raised by either team during each competition attempt.

Technical Rules

- 19) During each competition attempt, the Lunabot is limited to autonomous and telerobotic operations only. No physical access to the Lunabot will be allowed during each competition attempt. In addition, telerobotic operators are only allowed to use data and video originating from the Lunabot and the NASA video monitors. Visual and auditory isolation of the telerobotic operators from the Lunabot in the Mission Control Center is required during each competition attempt. Telerobotic operators will be able to observe the LunArena through overhead cameras in the LunArena through monitors that will be provided by NASA in the Mission Control Center. These color monitors should be used for situational awareness only. No other outside communication via cell phones, radios, other team members, etc. is allowed in the Mission Control Center once each competition attempt begins.
- 20) The Lunabot mass is limited to a maximum of 80.0 kg. Subsystems on the Lunabot used to transmit commands/data and video to the telerobotic operators are counted toward the 80.0 kg mass limit. Equipment not on the Lunabot used to receive data from and send commands to the Lunabot for telerobotic operations is excluded from the 80.0 kg mass limit.
- 21) The Lunabot must provide its own onboard power. No facility power will be provided to the Lunabot. There are no power limitations except that the Lunabot must be self-powered and included in the maximum Lunabot mass limit of 80.0 kg.
- 22) The Lunabot must be equipped with an easily accessible <u>red</u> emergency stop button (kill switch) of minimum diameter five cm on the surface of the Lunabot requiring no steps to access. The emergency stop button must stop the Lunabot's motion and disable all power to the Lunabot with one push motion on the button. It must be

highly reliable and instantaneous. For these reasons an unmodified "Commercial Off-The-Shelf" (COTS) red button is required. A closed control signal to a mechanical relay is allowed as long as it stays open to disable the Lunabot. The reason for this rule is to completely safe the Lunabot in the event of a fire or other mishap. The button should disconnect the batteries from all controllers (high current, forklift type button) and it should isolate the batteries from the rest of the active sub-systems as well.

23) The communications rules used for telerobotic operations follow:

A. LUNABOT WIRELESS LINK

- 1. Each team will provide the wireless link (access point, bridge, or wireless device) to their Lunabot, which means that each team will bring the Wi-Fi equipment/router and set their own IP addresses.
 - a. NASA will provide an elevated network drop (Female RJ-45 Ethernet jack) in the LunArena that extends to the Mission Control Center, where NASA will provide a network switch for the teams to plug in their laptops.
 - i. The network drop in the LunArena will be elevated high enough above the edge of the regolith bed wall to provide adequate radiofrequency visibility of the LunArena.
 - ii. A shelf will be setup next to the network drop and located 4 to 6 feet off the ground and will be no more than 50 feet from the Lunabot. This shelf is where teams will place their Wireless Access Point (WAP) to communicate with their Lunabot. The distance from the LunArena to the Mission Control Center will be around 150 200 feet.
 - iii. The WAP shelves for side A and side B of the LunArena will be no closer than 25' from each other to prevent electromagnetic interference (EMI) between the units.
 - b. NASA will provide a standard 110VAC outlet by the network drop. Both will be no more than 2 feet from the shelf.
 - c. During setup time before the match starts the teams will be responsible for setting up their access point.
- 2. The teams must use the USA IEEE 802.11 b/g standard for their wireless connection (WAP and rover client). Teams cannot use multiple channels for data transmission. Encryption is not required but it is highly encouraged to prevent unexpected problems with team links.
 - a. During a match, one team will operate on channel 1 and the other team will operate on channel 11.
 - b. The channel assignments will be made upon team check-in with the LunaPit crew chief.
- 3. Each team will be assigned an SSID that they must use for their wireless equipment.
 - a. SSID will be "Team ##"
 - b. Teams will broadcast their SSID
- 4. Bandwidth constraints:
 - a. Teams will be awarded the Efficient Use of Communications Power Award for using the least amount of average bandwidth during the timed and NASA monitored portion of the competition.
 Teams must collect the minimum 10 kg of BP-1 to qualify for this award.
 - b. The communications link is required to have an <u>average</u> bandwidth of no more than 5 megabits per second. There will not be a <u>peak</u> bandwidth limit.

B. RF & COMMUNICATIONS APPROVAL

- 1. Each team must demonstrate to the communication judges that their Lunabot and access point is operating only on their assigned channel. Each team will have approximately 15 minutes at the communication judge's station.
- 2. To successfully pass the communications judge's station a team must be able to command their Lunabot (by driving a short distance) from their Lunabot driving/control laptop through their wireless access point. The judges will verify this and use the appropriate monitoring tools to verify that the teams are operating only on their assigned channel.
- 3. If a team cannot demonstrate the above tasks in the allotted time, the team will be disqualified from the competition.
- 4. Each team will receive an assigned time from the LunaPit crew chief, on a first come, first serve basis, on Monday, May 21, 2012 or Tuesday, May 22, 2012 to show the communication judges their compliance with the rules.
- 5. The NASA communications technical experts will be available to help teams make sure that they are ready for the communication judge's station on Monday, May 21, 2012 or Tuesday, May 22, 2012.

- 6. Once the team arrives at the communication judge's station, the team can no longer receive assistance from the NASA communications technical experts.
- 7. If a team is on the wrong channel during their competition attempts, the team will be required to power down and be disqualified.

C. WIRELESS DEVICE OPERATION IN THE PITS

- 1. Teams will not be allowed to power up their transmitters on any frequency in the Lunapits during the practice matches or competition attempts. All teams must have a hard-wired connection for testing in the Lunapits.
- 2. There will be designated times for teams to power up their transmitters when there are no practice matches underway.
- 24) The Lunabot must be contained within 1.5 m length x 0.75 m width x 0.75 m height. The Lunabot may deploy or expand beyond the 1.5 m x 0.75 m footprint after the start of each competition attempt, but may not exceed a 1.5 meter height. The Lunabot may not pass beyond the confines of the outside wall of the LunArena and the LunaBin during each competition attempt to avoid potential interference with the surrounding tent. The team must declare the orientation of length and width to the inspection judge. Because of actual lunar hardware requirements, no ramps of any kind will be provided or allowed. An arrow on the reference point must mark the forward direction of the Lunabot in the starting position configuration. The judges will use this reference point and arrow to orient the Lunabot in the randomly selected direction and position. A multiple robot system is allowed but the total mass and starting dimensions of the whole system must comply with the volumetric dimensions given in this rule.
- 25) To ensure that the Lunabot is usable for an actual lunar mission, the Lunabot cannot employ any fundamental physical processes (e.g., suction or water cooling in the open lunar environment), gases, fluids or consumables that would not work in the lunar environment. For example, any dust removal from a lens or sensor must employ a physical process that would be suitable for the lunar surface. Teams may use processes that require an Earth-like environment (e.g., oxygen, water) only if the system using the processes is designed to work in a lunar environment and if such resources used by the Lunabot are included in the mass of the Lunabot. Pneumatic mining systems are allowed only if the gas is supplied by the Lunabot itself.
- 26) Components (i.e. electronic and mechanical) are not required to be space qualified for the lunar vacuum, electromagnetic, and thermal environments. Since budgets are limited, the competition rules are intended to require Lunabots to show lunar plausible system functionality but the components do not have to be traceable to a space qualified component version. Examples of allowable components are: Sealed Lead-Acid (SLA) or Nickel Metal Hydride (NiMH) batteries; composite materials; rubber or plastic parts; actively fan cooled electronics; motors with brushes; and proximity detectors and/or Hall Effect sensors, but proceed at your own risk since the BP-1 is very dusty. Teams may use honeycomb structures as long as they are strong enough to be safe. Teams may not use rubber pneumatic tires; air/foam filled tires; ultra sonic proximity sensors; or hydraulics because NASA does not anticipate the use of these on a lunar mission.
- 27) The Lunabot may not use any process that causes the physical or chemical properties of the BP-1 to be changed or otherwise endangers the uniformity between competition attempts.
- 28) The Lunabot may not penetrate the BP-1 surface with more force than the weight of the Lunabot before the start of each competition attempt.
- 29) No ordnance, projectile, far-reaching mechanism (adhering to Rule 24), etc. may be used. The Lunabot must move on the BP-1 surface.
- 30) No team can intentionally harm another team's Lunabot. This includes radio jamming, denial of service to network, BP-1 manipulation, ramming, flipping, pinning, conveyance of current, or other forms of damage as decided upon by the judges. Immediate disqualification will result if judges deem any maneuvers by a team as being offensive in nature. Erratic behavior or loss of control of the Lunabot as determined by the judges will be cause for immediate disqualification. A judge may disable the Lunabot by pushing the <u>red</u> emergency stop button at any time.
- 31) Teams must electronically submit documentation containing a description of their Lunabot, its operation, potential safety hazards, a diagram, and basic parts list by April 30, 2012 at 12:00 p.m. (noon) eastern time in the United States.

32) Teams must electronically submit video documentation containing no less than 30 seconds but no more than 5 minutes of their Lunabot in operation for at least one full cycle of operation by April 30, 2012 at 12:00 p.m. (noon) eastern time in the United States. One full cycle of operations includes excavation and depositing material. This video documentation is solely for technical evaluation of the Lunabot.

Video Specifications/Formats/Containers: .avi, .mpg, .mpeg, .ogg, .mp4, .mkv, .m2t, .mov; Codecs: MPEG-1, MPEG-2, MPEG-4 (including AVC/h.264), ogg theora; Minimum frame rate: 24 fps; Minimum resolution: 320 x 240 pixels

Shipping

33) Teams may ship their Lunabots to <u>arrive no earlier than May 14, 2012</u>. The Lunabots will be held in a safe, unairconditioned area and be placed in the team's LunaPit by Monday, May 21, 2012. The shipping address is:

Kennedy Space Center Visitor Complex Lunabotics Mining Competition Mail Code: DNPS Kennedy Space Center, FL 32899

34) Return shipping arrangements must be made <u>prior</u> to the competition. All Lunabots must be picked up from the Kennedy Space Center Visitor Complex no later than 5:00 p.m. on Tuesday, May 29, 2012. Any abandoned Lunabots will be discarded after this date.

LunArena Diagrams

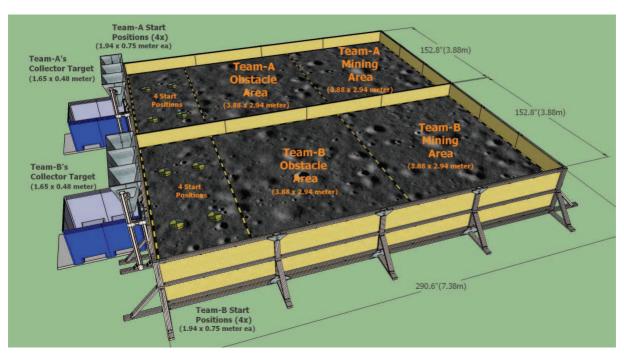


Diagram 1: LunArena (isometric view)

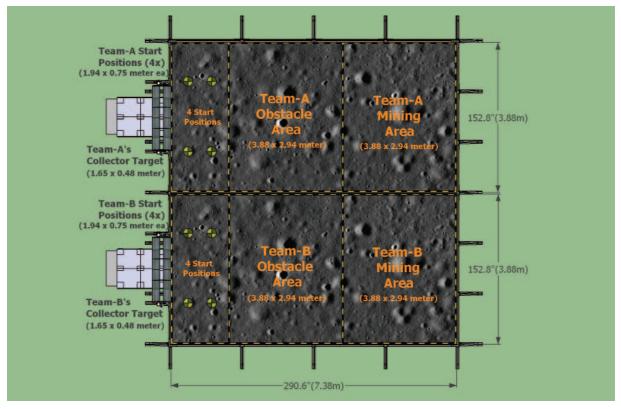


Diagram 2: LunArena (top view)

LunaBin Diagram

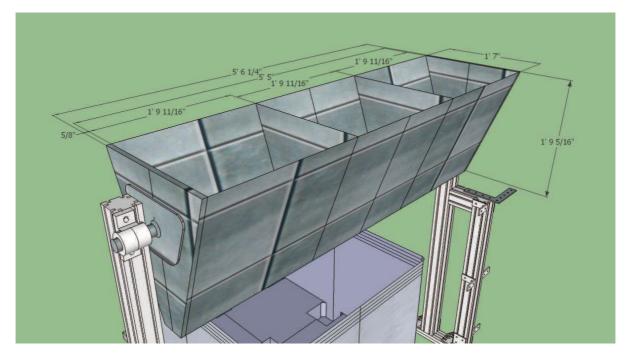


Diagram 3: LunaBin

Lunabotics Systems Engineering Paper

Each team must submit a Systems Engineering Paper electronically in PDF by April 23, 2012 at 12:00 p.m. (noon) eastern time in the United States. Cover page must include: team name, title of paper, full names of all team members, university name and faculty advisor's full name. **Appendices are not allowed.** All pertinent information required in the rubric must be in the body of the paper. A minimum score of 15 out of 20 possible points must be achieved to qualify to win in this category. In the case of a tie, the judges will choose the winning Systems Engineering Paper. The judges' decision is final. The team with the winning Systems Engineering Paper will receive a team plaque, individual certificates, and a \$500 team scholarship. Second and third place winners will receive individual team certificates.

For reference, the NASA Systems Engineering Handbook is available at: http://education.ksc.nasa.gov/esmdspacegrant/LunarRegolithExcavatorCourse/Site%20Documents/NASA%20SP-2007-6105.pdf.

Lunab	ootics Systems E	ngineering Pape	r Scoring Rubric	;	
Elements	4	3	2	1	0
Formatted professionally, clearly organized, correct grammar and spelling, maximum of 20 pages not counting the cover and source pages only; 12 font size; single spaced. No appendices allowed. Cover page Introduction Purpose Sources	All five elements are exceptionally demonstrated	Five elements are clearly demonstrated	Four elements are clearly demonstrated	Three or less elements are clearly demonstrated	Zero elements are clearly demonstrated
Intrinsic Merit: Deliverables identified Budget Schedule Major reviews: system requirements, preliminary design and critical design Illustrations support the technical content	All five elements are exceptionally demonstrated	Five elements are clearly demonstrated	Four elements are clearly demonstrated	Three or less elements are clearly demonstrated	Zero elements are clearly demonstrated
Technical Merit:	One point fo	or each element exc	ceptionally demons	trated up to twelv	re points.

Lunabotics Outreach Project Report

Each team must participate in an educational outreach project in their local community. Outreach examples include actively participating in school career days, science fairs, technology fairs, extracurricular science or robotic clubs, or setting up exhibits in local science museums or a local library. Other ideas include organizing a program with a Boys and Girls Club, Girl Scouts, Boy Scouts, etc. Teams are encouraged to have fun with the outreach project and share knowledge of science, robotics and engineering with the local community.

Each team must submit a report of the Lunabotics Outreach Project electronically in PDF by April 23, 2012 at 12:00 p.m. (noon) eastern time in the United States. Cover page must include: team name, title of paper, full names of all team members, university name and faculty advisor's full name. A minimum score of 15 out of 20 possible points must be achieved to qualify to win in this category. In the case of a tie, the judges will choose the winning outreach project. The judges' decision is final. The team with the winning outreach project will receive a team plaque, individual certificates, and a \$500 team scholarship. Second and third place winners will receive individual team certificates.

	Lunabotics Outreach Project Scoring Rubric									
Elements	4	3	2	1	0					
Content: Introduction Outreach recipient group identified Purpose Cover page	All four elements are exceptionally demonstrated	Four elements are clearly demonstrated	Three elements are clearly demonstrated	Two elements are clearly demonstrated	Zero elements are clearly demonstrated					
Inspires others to learn about robotics, engineering or lunar activities Quality of the outreach Utilizes hands-on activities	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two elements are clearly demonstrated	One element is clearly demonstrated	Zero elements are clearly demonstrated					
Creativity: Inspirational Engages others in robotics, engineering or lunar activities Material corresponds to audience's level of understanding	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two elements are clearly demonstrated	One element is clearly demonstrated	Zero elements are clearly demonstrated					
Illustrations and Media:	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two elements are clearly demonstrated	One element is clearly demonstrated	Zero elements are clearly demonstrated					
Correct grammar and spelling Five-page limit (cover page and appendices excluded in page count) Clearly organized	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two elements are clearly demonstrated	One element is clearly demonstrated	Zero elements are clearly demonstrated					

Lunabotics Slide Presentation and Demonstration

The Lunabotics Slide Presentation is an optional category in the overall competition. The presentation and demonstration must be no more than 20 minutes with an additional 5 minutes for questions and answers. It will be judged at the competition in front of an audience including NASA and private industry judges. The presentations must be submitted electronically in PDF by April 23, 2012 at 12:00 p.m. (noon) eastern time in the United States. A cover slide must contain the team name, title of presentation, full names of all team members, university name, and faculty advisor's full name. A minimum score of 18 out of 24 possible points must be achieved to qualify to win in this category. In the case of a tie, the judges will choose the winning presentation. The judges' decision is final. The team with the winning presentation will receive a team plaque, individual team certificates, and a \$500 team scholarship. Second and third place winners will receive individual team certificates.

	Lunabotics Slide Presentation Scoring Rubric								
Elements	4	3	2	1	0				
Content:	All four elements are exceptionally demonstrated	Four elements are clearly demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
Technical Merit:	elements are exceptionally	Six elements are clearly demonstrated	Five elements are clearly demonstrated	Four or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
Creativity: Innovative Inspirational Engaging Highlights what make the Lunabot design unique	All five elements are exceptionally demonstrated	Five elements are clearly demonstrated	Four elements are clearly demonstrated	Three or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
infuses personality Illustrations and Media:									
 Appropriate Supports the technic content Shows progression of project Clearly presents 	exceptionally	Four elements are clearly demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
design of Lunabot									
 Formatting and Appearance Proper grammar Correct spelling Readable Aesthetically pleasing 	elements are exceptionally demonstrated	Four elements are clearly demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
Presentation:									
 Makes presentation accompetition Demonstrates Lunabunder hardwire and pendent control during presentation Engages audience 	All four elements are exceptionally	Four elements are clearly demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated				
 Answers questions 									

Lunabotics Team Spirit

Lunabotics Team Spirit is an optional category in the overall competition. A minimum score of 12 out of 15 possible points must be achieved to qualify to win in this category. In the case of a tie, the judges will choose the winning team. The judges' decision is final. The team winning the Team Spirit Award at the Lunabotics Mining Competition will receive a team plaque, individual certificates, and a \$500 team scholarship. Second and third place winners will receive individual team certificates.

Luna	Lunabotics Team Spirit Competition Scoring Rubric								
Elements	3	2	1	0					
Exhibits teamwork in and out of the LunArena Exhibits a strong sense of collaboration within the team Supports other teams with a healthy sense of competition	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated					
Exudes a positive attitude in all interactions, not limited to competition attempt Demonstrates an infectious energy Motivates and encourages team Keeps pit clean and tidy at all times	All four elements are exceptionally demonstrated	Four elements are clearly demonstrated	Three or less elements are clearly demonstrated	Zero elements are clearly demonstrated					
Demonstrates creativity Wears distinctive team shirts or hats Decorates team's LunaPit to reflect school/team spirit	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated					
Engages: Engages audience in team spirit activities Engages other teams in team spirit activities Makes acquaintances with members of other teams	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated					
Demonstrates originality in team activities Displays originality in the team name Displays originality in the team logo	All three elements are exceptionally demonstrated	Three elements are clearly demonstrated	Two or less elements are clearly demonstrated	Zero elements are clearly demonstrated					

Categories for Bonus Points

Collaboration between a majority school with a designated United States Minority Serving Institution Collaboration between a majority school and a designated U.S. minority serving institution (MSI) must be identified by November 30, 2011. MSI student team members must submit their student participant forms and transcripts and be indicated on the team roster by January 31, 2012 at 12:00 p.m. (noon) eastern time in the United States to receive the 10 bonus points. A list of U.S. minority serving institutions may be found at: http://www2.ed.gov/about/offices/list/ocr/edlite-minorityinst.html.

Multidisciplinary Engineering Teams

Team members from each different science, technology, engineering or mathematics (STEM) discipline* will count for one bonus point up to a maximum of ten. Disciplines will be indicated on the student participant form by January 31, 2012 at 12:00 p.m. (noon) eastern time in the United States. No bonus points will be given in this category if a team has only one discipline represented. If a member of the team is in a STEM discipline that is not on this list, the team lead or faculty advisor may e-mail Susan.G.Sawyer@nasa.gov` to request approval of that discipline for the competition.

Aeronautical Engineering
Aerospace Engineering

Astrobiology

Astronautical Engineering

Astronomy Astrophysics

Atmospheric Sciences

Bacteriology Biochemistry Biology Biophysics

Chemical Engineering

Chemistry

Civil Engineering
Computer Engineering
Computer Science
Electrical Engineering
Engineering Management

Environmental Engineering

Geography

Geological Engineering

Geosciences Health Engineering

Industrial/Manufacturing Engineering

Information Technology

Materials/Metallurgical Engineering

Mathematics

Mechanical Engineering

Microbiology Mining Engineering

Natural Resource Management

Nuclear Engineering Oceanography

Optics Physics

Software Engineering Systems Engineering

Mined and Deposited BP-1

Teams not winning first, second, or third place in the mining category can earn one bonus point toward the Joe Kosmo Award for Excellence for each kilogram of BP-1 mined and deposited up to a maximum of ten points during their competition attempts.

^{*}Team members may be from other disciplines, but only STEM disciplines are awarded bonus points.

Categories & Awards

In addition to the awards listed below, school plaques and/or individual team certificates will be awarded for exemplary performance in the following categories:

Category	Required/ Optional	Due Dates	Award	Maximum Points toward Joe Kosmo Award for Excellence
On-site Mining in the LunArena	Required	May 23-26, 2012	First place \$3,000 team scholarship and Kennedy launch invitations	30
			Second place \$2,000 team scholarship and Kennedy launch invitations	25
			Third place \$1,000 team scholarship and Kennedy launch invitations	20
			Teams not placing 1 st , 2 nd , or 3 rd will receive one point per kilogram mined and deposited up to 10 points	Up to 10
Systems Engineering Paper	Required	April 23, 2012	\$500 team scholarship	Up to 20
Outreach Project Report	Required	April 23, 2012	\$500 team scholarship	Up to 20
Slide Presentation and Demonstration	Optional	April 23, 2012 and On-Site on May 23-26, 2012	\$500 team scholarship	Up to 24
Team Spirit Competition	Optional	All Year	\$500 team scholarship	Up to 15
Collaboration With a Minority Serving Institution	Optional	Nov. 30, 2011		10 bonus points
Multidisciplinary Team	Optional	Jan. 31, 2012		Up to 10 bonus points
Joe Kosmo Award for Excellence	Grand Prize for Most Points	All Year	A school trophy, \$5,000 team scholarship, KSC launch invitations, and up to \$1,000 travel expenses for each team member and one faculty advisor to attend one of NASA's remote research and technology tests	Total of above points, maximum of 129 points possible
Judges' Innovation Award	Optional	May 23-26, 2012	A school trophy	
Efficient Use of Communications Power Award	Optional	May 23-26, 2012	A school trophy	

Lunabotics Checklist

Required Competition Elements

If required elements are not received by the due dates, then the team is not eligible to compete in any part of the competition (NO EXCEPTIONS).

	Registration Application*	November 30, 2011
	Systems Engineering Paper	April 23, 2012
	Outreach Project Report	April 23, 2012
	On-site Mining	May 21-26, 2012
	 Team Check-in, Unload/Uncrate Lunabot 	May 21 & 22, 2012 by noon
	 Practice Days 	May 21-23, 2012
	Competition Days	May 23-26, 2012
	 Awards Ceremony 	May 26, 2012 (evening)
Option	al Competition Elements	
	Presentation File	April 23, 2012
	Team Spirit	All year
Requir	red Documentation	
	Registration Application	November 30, 2011
	Letter of Support from lead university's Dean of Engineering	November 30, 2011
	Letter of Support from lead university's Faculty Advisor	November 30, 2011
	MSI Collaboration Notification	November 30, 2011
	Team Roster with MSI students indicated	January 31, 2012
	Student Participant Form	January 31, 2012
	Faculty Form	January 31, 2012
	Transcripts (unofficial copy is acceptable)**	January 31, 2012
	Signed Media Release Form	January 31, 2012
	Request for Team Invitation Letter for International Teams***	February 24, 2012
	Team Photo including faculty (high resolution .jpg format preferred)	March 30, 2012
	Team Biography (200 words maximum)	March 30, 2012
	Head Count Form	March 30, 2012
	Revised Team Roster (no changes accepted after this date)	March 30, 2012
	Rule 31 documentation	April 30, 2012
	Rule 32 video	April 30, 2012
Option	al Documentation	
	Student Resume (optional)	January 31, 2012

^{*}Registration is limited to the first 60 approved teams. Registration is limited to one team per university campus. Internationally, registration is limited to 10 teams per country. Registration will end when NASA approves 60 applications or on November 30, 2011, whichever occurs first.

**Each student's Transcript or Statement of Marks must be from the university and show:

- name of university
- name of student
- major course of study
- current student status within the 2011-2012 academic year
- · coursework taken and grades

***International team's invitation letters for visa request purposes will be mailed during the week of February 27, 2012 with only the names of faculty advisors and student team members on the team roster who have completed their participant forms and submitted their transcripts or statement of marks. NASA will not provide individual letters.

All documents are due by 12:00 p.m. (noon) eastern time in the United States.

Definitions

<u>Autonomous</u> – The operation of a team's Lunabot with no human interaction.

<u>Black Point-1 (BP-1)</u> – A crushed lava aggregate with a natural particle size distribution similar to that of lunar soil. The aggregate will have a particle size and distribution similar to the lunar regolith as stated in the <u>Lunar Sourcebook: A User's Guide to the Moon</u>, edited by G. H. Heiken, D. T. Vaniman, and B. M. French, copyright 1991, Cambridge University Press. Teams are encouraged to develop or procure simulants based on lunar type of minerals and lunar regolith particle size, shape, and distribution.

<u>Competition attempt</u> – The operation of a team's Lunabot intended to meet all the requirements for winning the mining category by performing the functional task. The duration of each competition attempt is 10-minutes.

<u>Excavated mass</u> – Mass of the excavated BP-1 deposited to the LunaBin by the team's Lunabot during each competition attempt, measured in kilograms (kg) with official result recorded to the nearest one tenth of a kilogram (0.1 kg).

<u>Functional task</u> – The excavation of BP-1 from the LunArena by the Lunabot and deposit of BP-1 from the Lunabot into the LunaBin.

<u>Minimum excavation requirement</u> – 10.0 kg is the minimum excavated mass which must be met in order to qualify to win the competition.

<u>Practice time</u> – Teams will be allowed to practice with their Lunabots in the LunArena. NASA technical experts will offer feedback on real-time networking performance during practice attempt. Only one practice attempt is required and guaranteed.

<u>Reference point</u> – A fixed location signified by an arrow showing the forward direction on the Lunabot that will serve to verify the starting orientation of the Lunabot within the LunArena.

<u>LunaBin</u> – A collector bin in NASA's Lunabotics Mining Competition provided by NASA for each competition attempt into which each team will deposit excavated BP-1. The LunaBin will be large enough to accommodate each team's excavated BP-1. The LunaBin will be stationary and located adjacent to the LunArena. See Diagram 3.

<u>Lunabot</u> – A teleoperated or autonomous robotic excavator in NASA's Lunabotics Mining Competition including mechanical and electrical equipment, batteries, gases, fluids and consumables delivered by a team to compete in the competition.

<u>LunaPoints</u> – Points earned from the two competition attempts in NASA's Lunabotics Mining Competition will be averaged to determine ranking in the on-site mining category.

 $\underline{\text{LunArena}}$ – An open-topped container (i.e., a box with a bottom and 4 side walls only), containing BP-1, within which the Lunabot will perform each competition attempt. The inside dimensions of the each side of the LunArena will be 7.38 meters long and 3.88 meters wide, and 1 meter in depth. The BP-1 aggregate will be less than one meter in depth. A dividing wall will be in the center of the LunArena. The LunArena for the practice days and official competition will be provided by NASA. The LunArena will be outside in an enclosed tent. The LunArena lighting will consist of artificial lamps inside a tent structure. Assume daylight conditions. The atmosphere will be an air-conditioned tent without significant air currents and cooled to approximately 77 degrees Fahrenheit. See Diagrams 1 – 3.

<u>Telerobotic</u> – Communication with and control of the Lunabot during each competition attempt must be performed solely through the provided communications link which is required to have a total average bandwidth of no more than 5.0 megabits/second on all data and video sent to and received from the Lunabot.

<u>Time Limit</u> – 10 minutes to set up the Lunabot in the LunArena, 10 minutes for the Lunabot to perform the functional task, and 5 minutes to remove the Lunabot.

maxon DC motor and maxon EC motor

Key information

The motor as an energy converter

The electrical motor converts electrical power P_{el} (current I and voltage U) into mechanical power P_{mech} (speed n and torque M). The losses that arise are divided into frictional losses, attributable to P_{mech} and in Joule power losses P_J of the winding (resistance R). Iron losses do not occur in the coreless maxon DC motors. In maxon EC motors, they are treated formally like an additional friction torque. The power balance can therefore be formulated as:

 $P_{el} = P_{mech} + P_{J}$

The detailed result is as follows

$$U \cdot I = \frac{\pi}{30\,000} \, n \cdot M + R \cdot I^2$$

Electromechanical motor constants

The geometric arrangement of the magnetic circuit and winding defines in detail how the motor converts the electrical input power (current, voltage) into mechanical output power (speed, torque). Two important characteristic values of this energy conversion are the speed constant k_n and the torque constant k_M . The speed constant combines the speed n with the voltage induced in the winding U_{ind} (=EMF). U_{ind} is proportional to the speed; the following applies:

$$n = k_n \cdot U_{ind}$$

Similarly, the torque constant links the mechanical torque ${\it M}$ with the electrical current ${\it I}$.

$$M = k \cup I$$

The main point of this proportionality is that torque and current are equivalent for the maxon motor.

The current axis in the motor diagrams is therefore shown as parallel to the torque axis as well.

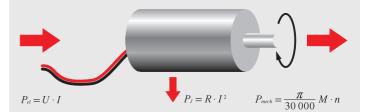
See also: Technology - short and to the point, explanation of the motor

Units

In all formulas, the variables are to be used in the units according to the catalog (cf. physical variables and their units on page 42).

The following applies in particular:

- All torques in mNm
- All currents in A (even no-load currents)
- Speeds (rpm) instead of angular velocity (rad/s)



Motor constants

Speed constant k_n and torque constant k_M are not independent of one another. The following applies:

$$k_{\scriptscriptstyle M} \cdot k_{\scriptscriptstyle M} = \frac{30\,000}{\pi}$$

The speed constant is also called specific speed. Specific voltage, generator or voltage constants are mainly the reciprocal value of the speed constant and describe the voltage induced in the motor per speed. The torque constant is also called specific torque. The reciprocal value is called specific current or current constant.

Motor diagrams

A diagram can be drawn for every maxon DC and EC motor, from which key motor data can be taken. Although tolerances and temperature influences are not taken into consideration, the values are sufficient for a first estimation in most applications. In the diagram, speed n, current l, power output P_2 and efficiency η are applied as a function of torque M at constant voltage U.

Speed-torque line

This curve describes the mechanical behavior of the motor at a constant voltage *U*:

- Speed decreases linearly with increasing torque.
- The faster the motor turns, the less torque it can provide.

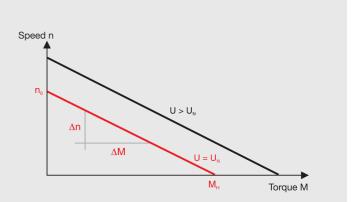
The curve can be described with the help of the two end points, no-load speed n_0 and stall torque M_H (cf. lines 2 and 7 in the motor data). DC motors can be operated at any voltage. No-load speed and stall torque change proportionally to the applied voltage. This is equivalent to a parallel shift of the speed-torque line in the diagram. Between the no-load speed and voltage, the following proportionality applies in good approximation

$$n_0 \approx k_n \cdot U$$

where k_n is the speed constant (line 13 of the motor data).

Independent of the voltage, the speed-torque line is described most practically by the slope or gradient of the curve (line 14 of the motor data).

$$\frac{\triangle n}{\triangle M} = \frac{n_0}{M_{\mu}}$$



Derivation of the speed-torque line

The following occurs if one replaces current I with torque M using the torque constant in the detailed power balance:

$$U \cdot \frac{M}{k_M} = \frac{\pi}{30\,000} \, n \cdot M + R \cdot \left(\frac{M}{k_M}\right)^{\frac{1}{2}}$$

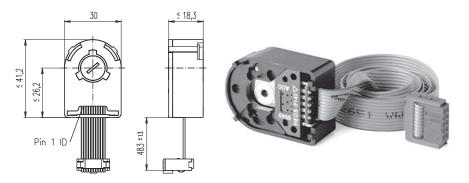
Transformed and taking account of the close relationship of k_{M} and k_{n} , an equation is produced of a straight line between speed n and torque M.

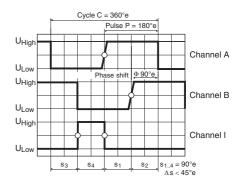
$$n = k_n \cdot U - \frac{30000}{\pi} \cdot \frac{R}{k_M^2} \cdot M$$

or with the gradient and the no-load speed n_0

$$n = n_0 - \frac{\Delta n}{\Delta M} \cdot M$$

Encoder HEDL 5540 500 CPT, 3 Channels, with Line Driver RS 422





Direction of rotation cw (definition cw p. 48)

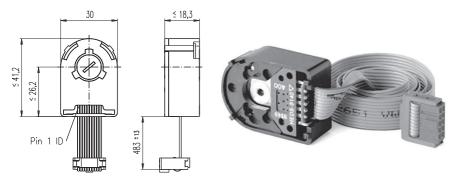
Stock program Standard program	Order Num	ber			
Special program (on request)	110512	110514	110516	h i	
Туре					
Counts per turn	500	500	500		
Number of channels	3	3	3		
Max. operating frequency (kHz)	100	100	100		- N. N.
Max. speed (rpm)	12000	12000	12000		
Shaft diameter (mm)	3	4	6		

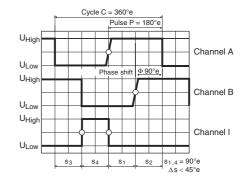
Shaft diamet	er (mm)					3	4	6	
maxon Modul	ar Sy <u>st</u> e	e m			_				
+ Motor	Page	+ Gearhead	Page	+ Brake	Page	Overall length [mm] / • see Gea	arhead	
RE 25	77/79					75.3	•		
RE 25	77/79	GP 26 / GP 32	227/229			•			
RE 25	77/79	KD 32, 1.0 - 4.5 Nm	235			•			
RE 25	77/79	GP 32, 0.75 - 6.0 Nm	230/232			•			
RE 25	77/79	GP 32 S	249-251			•			
RE 25, 20 W	79			AB 28	318	105.7			
RE 25, 20 W	79	GP 26 / GP 32	227/229	AB 28	318	•			
RE 25, 20 W	79	KD 32, 1.0 - 4.5 Nm	235	AB 28	318	•			
RE 25, 20 W	79	GP 32, 0.75 - 6.0 Nm	230/232	AB 28	318	•			
RE 25, 20 W	79	GP 32 S	249-251	AB 28	318	•			
RE 35, 90 W	81						91.7		
RE 35, 90 W	81	GP 32, 0.75 - 4.5 Nm	229				•		
RE 35, 90 W	81	GP 32, 0.75 - 6.0 Nm	231/232				•		
RE 35, 90 W	81	GP 32, 4.0 - 8.0 Nm	234				•		
RE 35, 90 W	81	GP 42, 3.0 - 15 Nm	237				•		
RE 35, 90 W	81	GP 32 S	249-251				•		
RE 35, 90 W	81			AB 28	318	124.2			
RE 35, 90 W	81	GP 32, 0.75 - 4.5 Nm	229	AB 28	318	•			
RE 35, 90 W	81	GP 32, 0.75 - 6.0 Nm	231/232	AB 28	318	•			
RE 35, 90 W	81	GP 42, 3.0 - 15 Nm	237	AB 28	318	•			
RE 35, 90 W	81	GP 32 S	249-251	AB 28	318	•			
RE 35, 90 W	81	GP 32, 4.0 - 8.0 Nm	234	AB 28	318	•			
RE 40, 150 W	82						91.7		
RE 40, 150 W	82	GP 42, 3.0 - 15 Nm	237				•		
RE 40, 150 W	82	GP 52, 4.0 - 30 Nm	240				•		
RE 40, 150 W	82			AB 28	318	124.2			
RE 40, 150 W	82	GP 42, 3.0 - 15 Nm	237	AB 28	318	•			
RE 40, 150 W	82	GP 52, 4.0 - 30 Nm	240	AB 28	318	•			
A-max 26	102-10					63.5			
A-max 26		8 GP 26, GS 30	227/228			•			
A-max 26		8 GP 32, 0.4 - 2.0 Nm	231			•			
A-max 26		8 GP 32, 0.75 - 6.0 Nm	230/233			•			
A-max 26		8 GS 38, 0.1 - 0.6 Nm	236			•			
A-max 26		8 GP 32 S	249-251			•			
A-max 32	110/11						82.3		
A-max 32		2 GP 32, 0.75 - 6.0 Nm	231/233				•		
A-max 32		2 GS 38, 0.1 - 0.6 Nm	236				•		
A-max 32	110/11:	2 GP 32 S	249-251				•		

Technical Data	Pin Allocation	Connection example
Supply voltage V_{CC} 5 V ± 10% Output signal EIA Standard RS 422 driver used: DS26LS31 Phase shift Φ 90°e ± 45°e Signal rise time (typically, at $C_L = 25$ pF, $R_L = 2.7$ k Ω , 25°C) 180 ns Signal fall time (typically, at $C_L = 25$ pF, $R_L = 2.7$ k Ω , 25°C) 40 ns Index pulse width 90°e Operating temperature range -40 +100°C Moment of inertia of code wheel ≤ 0.6 gcm² Max. angular acceleration 250 000 rad s² Output current per channel min20 mA, max. 20 mA Option 1000 Counts per turn, 2 Channels	1 N.C. 2 V _{cc} 3 GND 4 N.C. 5 Channel Ā 6 Channel B 7 Channel B 9 Channel I (Index) 10 Channel I (Index) Pin type Berg 246770 flat band cable AWG 28	Est V _{CC} Line receiver Recommended IC's: -MC 3486 -MC 3486

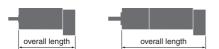
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Encoder HEDL 5540 500 CPT, 3 Channels, with Line Driver RS 422





	Direction of rotation cw (definition cw p. 48)				
Stock program Standard program Special program (on request)	Order Numl	ber			
Special program (on request)	110512	110514	110516	110518	
Туре					
Counts per turn	500	500	500	500	
Number of channels	3	3	3	3	
Max. operating frequency (kHz)	100	100	100	100	
Max. speed (rpm)	12000	12000	12000	12000	
Shaft diameter (mm)	3	4	6	8	



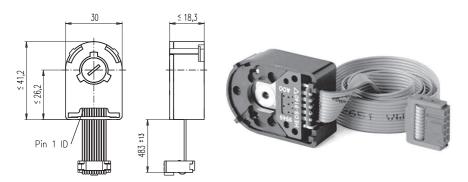


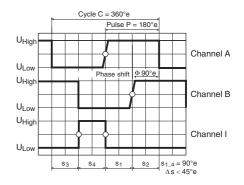
	. 0									
maxon Modula							. 1/-			
+ Motor	Page	+ Gearhead	Page	+ Brake	Page	Overall length	[mm] / • see Gea	arhead		
RE 50, 200 W	83								128.7	
RE 50, 200 W	83	GP 52, 4 - 30 Nm	241						•	
RE 50, 200 W	83	GP 62, 8 - 50 Nm	242						•	
RE 65, 250 W	84								157.3	
RE 65, 250 W	84	GP 81, 20 - 120 Nm	243						•	
EC 32, 80 W	154						78.4			
EC 32, 80 W	154	GP 32, 0.75 - 4.5 Nm	229				•			
EC 32, 80 W	154	GP 32, 0.75 - 6.0 Nm	231/233				•			
EC 32, 80 W	154	GP 32 S	249-251				•			
EC 40, 170 W	155							103.3		
EC 40, 170 W	155	GP 42, 3.0 - 15 Nm	237					•		
EC 40, 170 W	155	GP 52, 4.0 - 30 Nm	240					•		
EC-max 30, 40 W	166						62.6			
EC-max 30, 40 W	166	GP 32, 1 - 6 Nm	233				•			
EC-max 30, 40 W	166			AB 20	316		101.7			
EC-max 30, 40 W	166	GP 32, 1 - 6 Nm	233	AB 20	316		•			
EC-max 30, 40 W	166	GP 32 S					•			
EC-max 30, 40 W	166	GP 32, 4.0 - 8.0 Nm	234							
EC-max 30, 60 W	167						84.6			
EC-max 30, 60 W	167	GP 32, 4.0 - 8.0 Nm	234							
EC-max 30, 60 W	167	GP 42, 3 - 15 Nm	238				•			
EC-max 30, 60 W	167			AB 20	316		120.4			
EC-max 30, 60 W	167	GP 42, 3 - 15 Nm	238	AB 20	316		•			
,	168							81.4		
EC-max 40, 70 W	168	GP 42, 3 - 15 Nm	238					•		
EC-max 40, 70 W	168	,,,,,,		AB 28	317			121.4		
EC-max 40, 70 W	168	GP 42, 3 - 15 Nm	238	AB 28	317			•		
EC-max 40, 120 W								111.4		
EC-max 40, 120 W		GP 52, 4 - 30 Nm	241					•		
EC-max 40, 120 W		,, .		AB 28	317			140.8		
EC-max 40, 120 W		GP 52, 4 - 30 Nm	241	AB 28	317			•		

Technical Data	Pin Allocation	Connection example
Output signal driver used: DS Phase shift Φ 90° Signal rise time (typically, at C _L = 25 pF, R _L = 2.7 k Ω , 25°C) Signal fall time (typically, at C _L = 25 pF, R _L = 2.7 k Ω , 25°C) Index pulse width Operating temperature range 40 Moment of inertia of code wheel	S26LS31 O'e ± 45°e	Eine receiver Recommended IC's: - MC 3486 - SN 75175 - AM 26 LS 32 - AM 26 LS 32 - Channel A - Channel B - Channe

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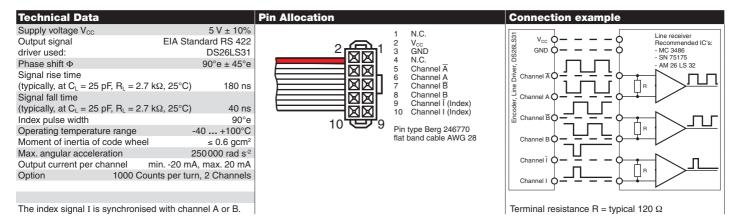
Encoder HEDL 5540 500 CPT, 3 Channels, with Line Driver RS 422





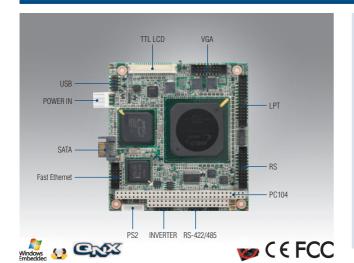
	Direction of rotation cw (definition cw p. 48)					
Stock program Standard program	Order Numl	ber				
Special program (on request)	110512	110514	110516			
Туре						
Counts per turn	500	500	500			
Number of channels	3	3	3			
Max. operating frequency (kHz)	100	100	100			
Max. speed (rpm)	12000	12000	12000			
Shaft diameter (mm)	3	4	6			

maxon Modu	ılar Svet	em .							
+ Motor	Page	+ Gearhead	Page	+ Brake	Page	Overall length [mm1/ • see Ge	arhead	
RE 25	78		. ago	· Ziano	. ago	63.8], = ==============================		
RE 25	78	GP 26 / GP 32	227/229)		•			
RE 25	78	KD 32. 1.0 - 4.5 Nm	235			•			
RE 25	78	GP 32, 0.75 - 6.0 Nm	230/232	2		•			
RE 25	78	GP 32 S	249-25	I		•			
RE 25, 20 W	78			AB 28	318	94.3			
RE 25, 20 W	78	GP 26 / GP 32	227/229	AB 28	318	•			
RE 25, 20 W	78	KD 32, 1.0 - 4.5 Nm	235	AB 28	318	•			
RE 25, 20 W	78	GP 32, 0.75 - 6.0 Nm	230/232	2 AB 28	318	•			
RE 25, 20 W	78	GP 32 S	249-25	I AB 28	318	•			
EC-4pole 22	173					70.1			
EC-4pole 22	173	GP 22 / GP 32	224/233	3		•			
EC-4pole 22	173	GP 32 S	249-25	I		•			
EC-4pole 22	174					87.5			
C-4pole 22	174	GP 22 / GP 32	224/233	3		•			
C-4pole 22	174	GP 32 S	249-25			•			
EC-4pole 30	175						67.6		
EC-4pole 30	175	GP 32, 4.0 - 8.0 Nm	234				•		
EC-4pole 30	175	GP 42, 3 - 15 Nm	238				•		
EC-4pole 30	175			AB 20	316		79.1		
EC-4pole 30	175	GP 32, 4.0 - 8.0 Nm	234	AB 20	316		•		
EC-4pole 30	175	GP 42, 3 - 15 Nm	238	AB 20	316		•		
EC-4pole 30	176						84.6		
EC-4pole 30	176	GP 32, 4.0 - 8.0 Nm	234				•		
EC-4pole 30	176	GP 42, 3 - 15 Nm	238				•		
EC-4pole 30	176			AB 20	316		96.1		
EC-4pole 30	176	GP 32, 4.0 - 8.0 Nm	234	AB 20	316		•		
EC-4pole 30	176	GP 42, 3 - 15 Nm	238	AB 20	316		•		
C-i 40, 50 W	190							49.0	
EC-i 40, 50 W	190	GP 32, 1 - 6 Nm	233					•	
EC-i 40, 50 W	190	GP 32 S	249-25	1				•	
EC-i 40, 70 W	191							59.0	
EC-i 40, 70 W	191	GP 32, 1 - 6 Nm	233					•	
EC-i 40, 70 W	191	GP 32 S	249-25					•	



PCM-3355

AMD LX800/LX600 PC/104 SBC, CRT, TTL, Ethernet, USB, COM, CFC



Features

- AMD low power LX800/500 MHz and LX600/366 MHz Processor
- 24-bit TFT LCD interface
- Supports compact size 96 x 90 mm PC/104 standard dimension
- Supports two RS-232, one RS-422/485, and two USB 2.0 ports
- Supports Embedded Software API and Utility

Software APIs:











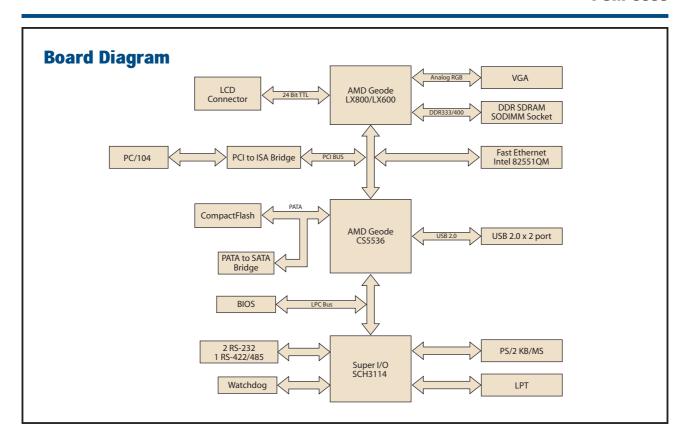
Utilities:





Specifications

-		
	CPU	AMD Geode™ LX800, 500 MHz/AMD Geode™ LX600, 366 MHz
	Frequency	500 MHz/ 366 MHz
Processor System	L2 Cache	128 KB
	System Chipset	AMD CS5536
	BIOS	Award 4-Mbit
	Technology	DDR 333/400 MHz
Memory	Max. Capacity	1 GB
	Socket	1 x 200-pin SODIMM
	Chipset	AMD Geode LX800/LX600
	VRAM	Optimized Shared Memory Architecture up to 64 MB system memory
Disalau	CDT	Supports up to 1920 x 1440 x 32 bpp at 85 Hz
Display	CRT	Supports up to 1600 x 1200 x 32 bpp at 100 Hz
	TTL LCD	Supports up to 1600 x 1200 x 32 bpp at 60 Hz for 24-bit single channel TFT
	Dual Display	CRT+TTL
	Speed	10/100 Mbps
Ethernet	Controller	Intel 82551QM
	Connector	Box Header
Watchdog Timer		Output System Reset
watchdog filler		Programmable counter from 1 ~ 255 minutes/ seconds
	CompactFlash	Compact Flash socket (Type I)
Storage	SATA	1 SATA, up to 1.5 Gb/s (150 MB/s) (Transfer from PATA)
	Floppy	1 82077AA compatible
	USB	2 x USB 2.0
	Serial	2 RS-232 from COM1/2, 1 RS-422/485 from COM3 (ESD protection for RS-232: Air gap ±15kV, Contact
Internal I/O	Serial	±8kV)
IIIIGIIIai I/O	Parallel (LPT)	1, IEEE 1284, EPP, and ECP compatible
	SMBus	1
	Keyboard/Mouse	1
Expansion	PC/104 slot	1
	Power Type	AT
	Power Supply Voltage	$\pm5\%$ only to boot up (12 V is optional for LCD inverter and add on card)
	Power Consumption (Typical)	LX800: 1.45 A @ +5 V, 2 mA @ +12 V
Power	Power Consumption	LX800: 1.74 A @ +5 V, 0.1 A @ +12 V
	(Max, test in HCT)	· · · · · · · · · · · · · · · · · · ·
	Power Management	ACPI/ APM1.2
	Battery	Lithium 3 V/210 mAH
Environment	Operational	0 ~ 60° C (32 ~ 140° F) (Operational humidity: 40° C @ 85% RH non-condensing)
LITTION	Non-Operational	-40° C ~ 85° C and 60° C @ 95% RH non-condensing
	Dimensions (L x W)	96 x 90 mm (3.8" x 3.5")
Physical Characteristics	Weight	0.097 kg (0.214 lb)
	Height	Top Side: 8.7 mm; Bottom Side: 10.6 mm



Ordering Information

Part No.	СРИ	Memory	TTL	SATA	Fast Ethernet	USB2.0	RS-232	RS-422/485	LPT/KB/MS	Expansion	Thermal Solution	Operating Temp.
PCM-3355F-L0A1E	AMD LX800	SODIMM	24-bit	Yes	1	2	2	1	Yes/Yes	PC/104	Passive	0 ~ 60° C
PCM-3355L-J0A1E	AMD LX600	SODIMM	24-bit	No	1	2	2	1	Yes/Yes	PC/104	Passive	0 ~ 60° C
PCM-3355Z-512LA1E	AMD LX800	512 MB bundle	24-bit	Yes	1	2	2	1	Yes/Yes	PC/104	Passive	-20 ~ 80° C
PCM-3355Z2-512LA1E	AMD LX800	512 MB bundle	24-bit	Yes	1	2	2	1	Yes/Yes	PC/104	Passive	-40 ~ 85° C

Note: Wide temp version has bundled with extended temperature grade memory module

Packing List

Part No.	Description	Quantity
	PCM-3355 SBC	
	Startup Manual	
	Utility CD	
1700060202	Cable 6P-6P-6P PS/2 KB & Mouse 20 cm	1
1700260250	LPT Port cable 25P to 26P 2.0 mm 25 cm	1
1703040157	RS-422/485 W/D-SUB COM 4P 15 cm	1
1703060053	PS2 Cable 6P (MINI-DIN)-6P (Wafer 2.0 mm) 6 cm	1
1703100121	USB 2-Port cable 10P 12 cm IDC 2.0 mm	1
1700008894	SATA data cable 7P 30 cm	1
1703150102	SATA power cable B4P-5.08/SATA 15P 10 cm	1
1701200220	RS-232 x 2 ports 2.0 mm 22 cm	1
1701160150	VGA Cable 15P to 16P 2.0 mm D-SUB 15 cm	1
1700005158	LAN cable RJ45 10P-2.0 mm 12 cm	1
9660104000	PC/104 screw and copper post package	1
1960016313T000	Heatsink for PCM-3355 (LX800/ LX600, 47.1 x 47.1 x 7.5 mm)	1
1960016315T000	Heatsink for PCM-3355 (CS5536, 22.7 x 22.8 x 6.3 mm)	1

Optional Accessories

Part No.	Description
165313222B	PC/104 connector 64-pin (Long pin)
165312022B	PC/104 connector 40-pin (Long pin)

Embedded OS/API

Embedded OS/API	Part No.	Description
WinCE	2070007869	Image CE 6.0 Pro PCM-3355 V1.2 ENG
Win XPE	2070007790	XPE WES2009 PCM-3355 Image GX3 V4.0 ENG
	2070007910	XPE WES2009 GX3 LX800 V4.0 MUI24
QNX		V6.3.2/ 6.4.1
Linux		Ubuntu 9.10
Software API	205E000019	SUSI 3.0 SW API for ESBC B: 20091116 XP

Value-Added Software Services

Software API: An interface that defines the ways by which an application program may request services from libraries and/or operating systems. Provides not only the underlying drivers required but also a rich set of user-friendly, intelligent and integrated interfaces, which speeds development, enhances security and offers add-on value for Advantech platforms. It plays the role of catalyst between developer and solution, and makes Advantech embedded platforms easier and simpler to adopt and operate with customer applications.

Software APIs

Control



General Purpose Input/Output is a flexible parallel interface that allows a variety of custom connections. It allows users to monitor the level of signal input or set the output status to switch on/off a device. Our API also provides Programmable GPIO, which allows developers to dynamically set the GPIO input or output status.



SMBus is the System Management Bus defined by Intel® Corporation in 1995. It is used in personal computers and servers for low-speed system management communications. The SMBus API allows a developer to interface a embedded system environment and transfer serial messages using the SMBus protocols, allowing multiple simultaneous device



I2C is a bi-directional two wire bus that was developed by Philips for use in their televisions in the 1980s. The I²C API allows a developer to interface with an embedded system environment and transfer serial messages using the I2C

protocols, allowing multiple simultaneous device control.



Monitor

A watchdog timer (WDT) is a device that performs a specific operation after a certain period of time if something goes wrong and the system does not recover on its own. A watchdog timer can be programmed to perform a warm boot

(restarting the system) after a certain number of seconds.



Hardware Monitor

The Hardware Monitor (HWM) API is a system health supervision API that inspects certain condition indexes, such as fan speed, temperature and voltage.



Hardware Control

The Hardware Control API allows developers to set the PWM (Pulse Width Modulation) value to adjust fan speed or other devices; it can also be used to adjust the LCD brightness.

Display



Brightness

The Brightness Control API allows a developer to interface with an embedded device to easily control brightness.



Power Saving

Make use of Intel SpeedStep technology to reduce power power consumption. The system will automatically adjust the CPU Speed depending on system loading.



The Backlight API allows a developer to control the backlight (screen) on/off in an embedded device.



System Throttling

Refers to a series of methods for reducing power consumption in computers by lowering the clock frequency. These APIs allow the user to lower the clock from 87.5% to 12.5%

Software Utilities



BIOS Flash

The BIOS Flash utility allows customers to update the flash ROM BIOS version, or use it to back up current BIOS by copying it from the flash chip to a file on customers' disk. The BIOS Flash utility also provides a command line version and API for fast implementation into customized applications.



Embedded Security ID

The embedded application is the most important property of a system integrator. It contains valuable intellectual property, design knowledge and innovation, but it is easily copied! The Embedded Security ID utility provides reliable security functions for customers to secure their application data within embedded



The Monitoring utility allows the customer to monitor system health, including voltage, CPU and system temperature and fan speed. These items are important to a device; if critical errors happen and are not solved immediately, permanent damage may be caused



eSOS

The eSOS is a small OS stored in BIOS ROM. It will boot up in case of a main OS crash. It will diagnose the hardware status, and then send an e-mail to a designated administrator. The eSOS also provides remote connection: Telnet server and FTP server, allowing the administrator to rescue the system.



Flash Lock

Flash Lock is a mechanism that binds the board and CF card (SQFlash) together. The user can "Lock" SQFlash via the Flash Lock function and "Unlock" it via BIOS while booting. A locked SQFlash cannot be read by any card reader or boot from other platforms without a BIOS with the "Unlock" feature.

PC/104 Datacom Modules



PCM-3643

4/8 RS-232 COM Port Module





PCM-3644

RS-232/422/485 COM Port Module



Specifications

General	
Bus Interface	PC/104 (ISA)
Chipset	Standard 16550, 16650, or 16750 compatible chipsets for serial ports
Channel	4/8 port RS-232 support
Baud Rate	50 ~ 115, 200 bps
Data Bits	5, 6, 7 or 8-bits
Stop Bit	1, 1.5, or 2
Parity	Even, odd, or none
Interrupt Level	IRQ 3, 4, 5, 6, 7, 9, 10, 11, 12 or 15
I/O Connector	40-pin header
Mechanical and Env	ironmental
Dimensions (L x W)	96 x 90 mm (3.8" x 3.5")
Weight	0.084 kg (0.185 lb)
Temperature	Operating: 0 ~ 60° C (32 ~ 140° F);
	Storage: -40 ~ 85° C (-10 ~ 185° F)
Operating Humidity	0% ~ 90% relative humidity, non-condensing
Power	
Power Supply Voltage	+5 V, ± 5 % tolerance on power supply
Power Consumption	+5 V @ 400 mA (typical)

Ordering Information

P/N	Description
PCM-3643-08A1E	8 x COM RS-232 Port Module
PCM-3643-04A1E	4 x COM RS-232 Port Module



PCM-3665

Dual GbE Module



Specifications

General	
Bus Interface	PC/104-Plus (PCI interface only)
Chipset	Intel® 82541PI (PCI 10/100/1000 Mbps)
Port	Single/Twin Ethernet port
Speed	10/100/1000 Mbps
Compatibility	PCI version 2.2, 33 MHz PCI
Mechanical and Envi	ironmental
Dimensions (L x W)	96 x 90 mm (3.8" x 3.5")
Weight	0.09 kg (0.198 lb)
Temperature	Operating: 0 ~ 60° C (32 ~ 140° F) Storage: -40 ~ 85° C (-10 ~ 185° F)
Operating Humidity	0% ~ 90% relative humidity, non-condensing
Power	
Power Consumption	Dual LAN: +5 V @ 1.2 A (typical) Single LAN: +5 V @ 0.6 A (typical)
Power Supply Voltage	+5 V, ±5 % tolerance on power supply

Ordering Information

P/N	Description
PCM-3665-00A1E	Dual GbE with RJ45 connector Module
PCM-3665P-00A1E	Dual GbE w/o RJ45 connector Module
PCM-3665-01A1F	Single GbF w/o R.145 connector Module

Specifications

General	
Bus Interface	PC/104-Plus (PCI interface only)
I/O Address	0 x 000 ~ 0 x 3F8
UART	4 x 16C550 (PCM-3614), 8 x 16C550 (PCM-3618)
IRQ	3, 4, 5, 6, 7, 9, 10, 11, 12, 15
Data Bits	5, 6, 7, 8
Stop Bits	1, 1.5, 2
Parity	none, even, odd
Speed (bps)	50 ~ 921.6 K
Connectors	4/8 DB-9 male
Signal Support	TxD+, TxD-, RxD CTS+, CTS-, RTS+ and RTS-
Surge Protection	1000 Vpc
Mechanical and Environmental	
Dimensions (L x W)	96 x 90 mm (3.8" x 3.5")
Weight	0.084 kg (0.185 lb)
Temperature	Operating: 0 ~ 60° C (32 ~ 140° F); Storage: -40 ~ 85° C (-10 ~ 185° F)
Operating Humidity	0% ~ 90% relative humidity, non-condensing
Power	
Power Supply Voltage	+5 V, ± 5 % tolerance on power supply
Power Consumption	+5 V @ 400 mA (typical)

Ordering Information

P/N	Description
PCM-3644-08A1E	8 x COM RS-232 Port Module
PCM-3644-04A1E	4 x COM RS-232 Port Module
PCM-3644H-04A1E	4 x COM RS-422 Port Module

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